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STATE-OF-THE-ART FOR ASSESSING **EARTHQUAKE HAZARDS IN THE UNITED STATES**

Report 12

CREDIBLE EARTHQUAKES FOR THE CENTRAL UNITED STATES

Otto W. Nuttli, Robert B. Herrmann Department of Earth and Atmospheric Sciences St. Louis University St. Louis, Missouri 63156

> December 1978 Report 12 of a Series

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20. ABSTRACT (Continued).

Pspecial study will be required for establishing credible ground-motion values for sites near the boundaries. A maximum-magnitude earthquake is determined for each zone, as well as a magnitude-recurrence equation. Using the Murphy-O'Brien formulation, as well as theoretical results of Herrmann and a limited amount of strong-motion data for the central United States, equations are derived for that region which relate maximum horizontal acceleration and velocity to body-wave magnitude and epicentral distance.



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PREFACE

This report was prepared by Drs. O. W. Nuttli and R. B. Herrmann, Department of Earth and Atmospheric Sciences, St. Louis University. It is part of ongoing work at the U. S. Army Engineer Waterways Experiment Station (WES) in Civil Works Investigation Study, "Methodologies for Selecting Design Earthquakes," sponsored by Office, Chief of Engineers, U. S. Army.

Preparation of this report was under the direction of Dr. E. L. Krinitzsky, Engineering and Rock Mechanics Division (EG&RMD), Geotechnical Laboratory (GL). General direction was by Mr. J. P. Sale, Chief, GL, and Dr. D. C. Banks, Chief, EG&RMD.

COL J. L. Cannon, CE, and Mr. F. R. Brown were Director and Technical Director, respectively, of WES during the period of this study.

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STATE-OF-THE-ART FOR ASSESSING EARTHQUAKE HAZARDS IN THE UNITED STATES

CREDIBLE EARTHQUAKES FOR THE CENTRAL UNITED STATES

PART I: THE CONCEPT OF THE CREDIBLE EARTHQUAKE

- earthquake-induced ground motion at a specific site. The one is deterministic, the other probabilistic. In the deterministic procedure one estimates the location and size of the earthquake of interest and then attenuates the source motion to the desired site. The resulting motion, which may be given as a time history, a response spectrum, or a set of ground-motion values (e.g., peak acceleration, peak ground velocity, peak displacement and bracketed duration) is called the credible earthquake motion. For critical structures, such as nuclear power plants and dams, whose failure could result in great loss of life and injury, as well as large economic loss, it is customary to assume that the credible earthquake occurs at the closest point to the site from the fault or the earthquake source region, and that the magnitude of the earthquake is the maximum which can be expected for the fault or for the source region.
- 2. For the probabilistic method one must identify the extent of all the earthquake source regions which can affect the site, and in addition must determine both the maximum-magnitude earthquake

which can occur in each source region and the magnitude-frequency recurrence rate of earthquakes for each source region. This information, together with a knowledge of the attenuation of wave energy for the region in question, can be used to make a probabilistic statement concerning the ground motion at the site, e.g., that there is a 10% probability that a horizontal ground acceleration as large as 0.25g will occur at the site in a 200-year period. The engineer, on the basis of his estimate of the criticalness of the structure and its expected lifetime, assigns the probability level and the time period and obtains from the analysis the ground-motion value which has that probability of occurrence in that selected number of years.

3. Both the deterministic and the probabilistic methods require that the seismic source zones be identified, that the maximum-magnitude earthquake for each source zone be estimated, that the magnitude-frequency recurrence rate for each source zone be determined and that the attenuation of seismic wave energy with distance be known as a function of wave frequency. A major part of this state-of-the-art report will be devoted to fulfilling these tasks for the central United States. (The central United States is defined as the area bounded on the west by the Rocky Mountain front and on the east by the Appalachians, excluding both mountain systems themselves.)

Thus the information contained in this report forms the basis for either deterministic or probabilistic assessment of earthquake ground motion in the central United States.

4. In keeping with the current practice of the Chief of Engineers and the Waterways Experiment Station of the Corps of Engineers, in this report the credible earthquake is taken to be the maximum-magnitude earthquake occurring at the nearest point in the source region to the site. If there are n source regions affecting the site, the effect of each of the n credible earthquakes must be considered in the process of defining the site specific credible earthquake. This study will define and provide justification for the maximum-magnitude earthquake for a source region as being the magnitude of the earthquake which has a 1000-year recurrence interval, or a 63% probability of occurring in a 1000-year period of time.

Justification for this definition will be given in Part IV: Regional Identification of Credible Earthquakes.

PART II: SOURCES OF INFORMATION ON CENTRAL UNITED STATES SEISMICITY

Felt Earthquakes

5. The history of earthquake activity in the central United
States begins with its settlement, which in some areas dates back to
the eighteenth century and in others to as recently as the late
nineteenth century. During the latter quarter of the nineteenth
century and subsequently, the U.S. Weather Bureau, the U.S. Coast and
Geodetic Survey, and related organizations in the Department of
Commerce and the U.S. Geological Survey have published annual lists

of earthquake activity. In general these included all earthquakes large enough to be felt by people, except in rural, sparsely populated areas where no reports were made of earth tremors. Prior to the late 1800's the historical record of earthquakes consists principally of newspaper accounts, and to a lesser extent of diaries and other personal accounts. Thus the record is incomplete, particularly for the smaller felt earthquakes. However, because of the large felt area associated with central United States earthquakes of body-wave magnitude 5 and greater, it is unlikely that any earthquakes of that size escaped attention since 1800.

6. Seismographs were first installed in the central United
States in the first decade of the twentieth century. The early
instruments were few in number and had a low magnification, so they
detected only earthquakes strong enough to be felt by people, and
not nearly all of them. In the 1930's Saint Louis University developed
a limited network of seismograph stations in the central Mississippi
valley, whose threshold of detectability (but not location ability)
was about the smallest earthquake that could be felt by humans. The
network provided valuable information on the velocities of seismic
waves and better epicentral locations than simple felt reports. The
next major step in the development of seismographic coverage of the
central United States came in the 1960's, when the World-Wide Standard
Seismograph Network was installed. The stations of this network,

although limited in number, had calibrated high-gain instruments with excellent time control. They provided valuable information on ground amplitudes and periods, and thus furnished the first usable material for determining the attenuation of seismic wave motion and for estimating magnitudes of earthquakes. Early in the 1970's microearthquake networks have been installed in a number of seismic source regions of the central United States. They have the capability of detecting the low magnitude, more frequently occurring earthquakes that are too small to be felt by man.

7. In order to assess the seismicity of a region, one must quantitatively describe the size of an earthquake as well as give its date, origin time and geographic location. In this report the body-wave magnitude, m_b, shall be used as the measure of the size of the earthquake. Since about 1962 body-wave magnitudes can be assigned to central United States earthquakes on the basis of the records of ground motion made by calibrated seismographs. Prior to that time, however, such data are lacking, and the magnitudes must be estimated by the effects of the earthquakes on people and on structures, i.e., by their Modified Mercalli (MM) intensity relations. Nuttli¹ developed a method for estimating m_b from the observed attenuation of MM intensity with distance for a given earthquake. He applied the method to the three principal earthquakes of the 1811-1812 sequence near New Madrid, Missouri. Since then Nuttli et al² have refined the methodology for determining m_b from intensity attenuation, and have

applied it to a number of earthquakes. This method works best for large historical earthquakes, of m_b equal to or greater than 5, for which adequate intensity data are available. It is estimated to give m_b values to \pm 0.2 units, as good as can be obtained from seismographic data. For smaller earthquakes Nuttli and Zollweg³ developed a relation between m_b and felt area, based on the data of recent earthquakes. This equa tion can be used for historical earthquakes for which the felt areas are known. It is estimated to give m_b values to \pm 0.3 units. Finally, there are many earthquakes for which only the epicentral intensity is known. For these Nuttli⁴ established an empirical relation between m_b and epicentral intensity, based on data of recent earthquakes for which both quantities are known. This method is estimated to give m_b values to \pm 0.5 units.

Microearthquakes

8. Microearthquakes are small magnitude earthquakes which cannot be felt by humans. They occur more frequently than larger magnitude earthquakes, so that in a relatively short time observation of them will yield useful seismological data. For example, they serve to outline the active fault zone, both laterally and with depth. They provide information on seismic wave velocity, and on the attenuation of the high frequency waves which principally are responsible for damage to structures. They also are useful for determining the predominant focal mechanism of the seismic region, which is related to

the state of stress and which provides information on the type of faulting, the strike and dip of the fault plane and the orientation of the slip motion. Finally, microearthquake data can be used to extend the magnitude-recurrence curve to the smaller magnitudes and thus give a better value of its slope and intercept.

- 9. The microearthquake network installed by Saint Louis University in southeast Missouri, northeast Arkansas, western Tennessee, western Kentucky and southern Illinois in 1974 was the first of its kind in the central United States. Figure 1 shows the location of the seismograph stations and the epicenters of the located earthquakes. From the figure the New Madrid fault zone is clearly outlined. It consists of a long southwest branch, of a very active central zone, and of a northeast-trending branch. Prior to the installation of the microearthquake network the New Madrid fault zone was thought to be broader and more diffuse. Now a main trend can be identified, although there are subparallel and other trends indicated by the data which broaden the earthquake source zone.
- 10. Since 1977 a number of additional microearthquake networks have been installed for the purpose of increasing knowledge of earthquake processes in the central United States. They include the Anna, Ohio region, the Wabash valley region, the states of Oklahoma and Kansas, and a small array in central Minnesota. At present the number of microearthquakes detected by these networks is insufficient

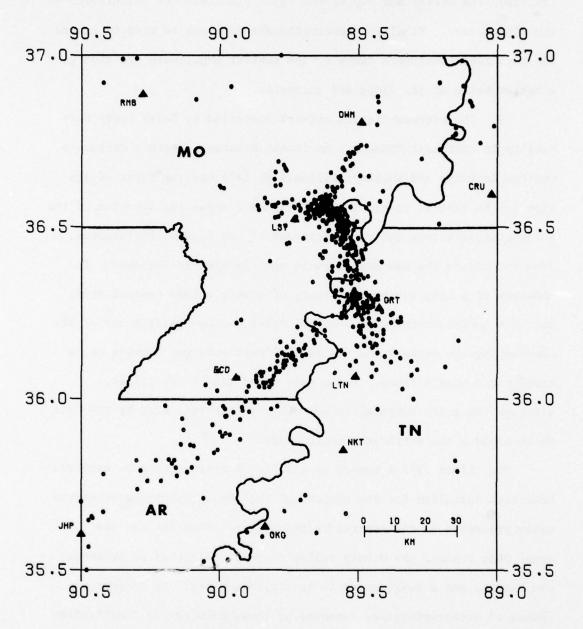


Figure 1. Earthquakes located in the central Mississippi valley between 1 July 1974 and 31 March 1978.

Triangles indicate seismograph stations. Small circles indicate earthquake epicenters

to draw any conclusions about the location of active fault zones in those regions. Due to the low rate of seismic activity, these arrays may have to operate for decades before a seismicity pattern as distinct as that shown in Figure 1 may be found.

1811-1812 New Madrid Earthquakes

- 11. The sequence of earthquakes that began in the central Mississippi valley on 16 December 1811 was unique, in regards to the magnitudes of the earthquakes, the number, size and duration of the aftershocks and the large damage and felt areas of the three major earthquakes of the sequence. Fuller⁵ described the physiographical effects of the earthquakes and Nuttli¹ the intensity distributions, magnitudes and ground motion. Recently, Nuttli et al² estimated the body-wave magnitudes of the three principal earthquakes to be 7.35 (16 December 1811), 7.2 (23 January 1812) and 7.5 (7 February 1812). The body-wave magnitude scale is saturated at these values. That is, no earthquake can have an mb value greater than about 7.5. Thus these earthquakes represent truly major events, similar to the great earthquakes occasionally associated with movements along lithospheric plate boundaries.
- 12. According to Fuller⁵, aftershocks continued until at least 1817. However, records of the number and size of the aftershocks were only kept for the three-month interval 16 December 1811 to 15 March 1812. During that time there were 207 damaging earthquakes, of m_b 5

or greater, and an additional 1667 that were large enough to be felt over an area of more than one county¹. Thus the 1811-1812 earthquakes provide dramatic evidence of the earthquake hazard which exists in the central United States.

Seismicity Map of Central United States

- 13. Figure 2 presents a map showing the epicenters of all known felt earthquakes (or earthquakes of $m_b \geq 3$) for the central United States through the year 1975. Excluded from the map are the thousands of aftershocks of the 1811-1812 earthquakes. The size of the symbol used in plotting the epicenters is proportional to the body-wave magnitude. In cases where several earthquakes had the same epicenter, they were plotted adjacent to each other in an area 10 km by 10 km, which is smaller than the area of uncertainty of location of most events. In cases where the 10 km by 10 km area became filled, the remaining epicenters were not plotted. This happened most frequently in the New Madrid seismic zone.
- 14. Data sources for Figure 2 and for the tables in Part III include Earthquake History of the United States⁶, United States

 Earthquakes⁷ for the years 1925 through 1972, Preliminary Determination of Epicenters⁸ for the years 1972 through 1974, Earthquakes of the Stable Interior, with Emphasis on the Midcontinent⁹, A Contribution to the Seismic History of Missouri¹⁰, Seismological Notes¹¹ for the years 1911 through 1975, Quarterly Seismological Bulletin of Saint Louis

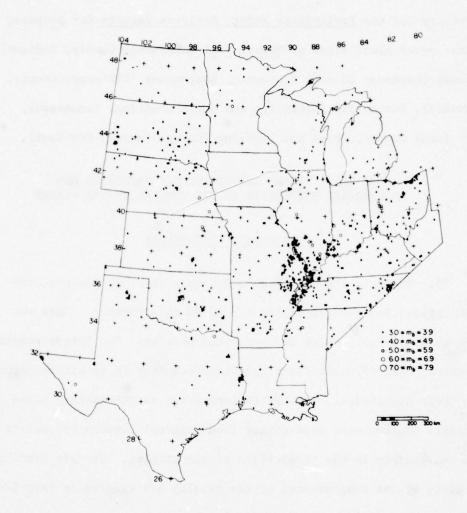


Figure 2. Map of felt earthquakes, or earthquakes of m_b = 3.0 or greater, for the central United States from historic times through 1975

University 12 for June 1974 through December 1975, unpublished lists of earthquakes compiled by J.E. Zollweg of Memphis State University, a list of earthquakes compiled by M.M. Varma and R.F. Blakely of Indiana University and the Preliminary Safety Analysis Reports for proposed nuclear power plant sites at Marble Hill (Jefferson County, Indiana), Calloway (Calloway County, Missouri), Koshkonong (Jefferson County, Wisconsin), Hartsville (Trousdale and Smith Counties, Tennessee), Perry (Lake County, Ohio) and Sterling (Cayuga County, New York).

PART III: RECENT RESULTS ON THE TECTONICS AND EARTHQUAKE ENERGETICS IN THE CENTRAL UNITED STATES

Patterns of Seismicity

- 15. The data shown in Figure 2 form a catalog, the contents of which will be found in Tables 1 10 in this chapter. Care was taken to avoid duplication and erroneous entries. The larger events are fairly well-documented and have been examined in detail to determine their magnitudes. Interpretations exist in the catalog since secondary sources were used rather than original references, due to time constraints in the preparation of the catalog. Certain statistical tests of the completeness of the catalog are applied in Part IV: Regional Identification of Credible Earthquakes.
- 16. The distribution of earthquake epicenters in Figure 2 and knowledge of the tectonic features of the central United States make it possible to identify the principal earthquake source zones.

Figure 3 shows the location and extent of these seismic source regions. The boundaries of the source zones are not as distinct as indicated. Rather, they represent regions in which damaging earthquakes have been known to occur. The boundary lines were selected in part for ease of the computer search. Thus, in designing for the ground motion at a specific site, judgment must be used if the site is near the boundary of a source zone. That is, the magnitude of the credible earthquake near the boundary of a source zone may, depending on individual circumstances, have a value as large as that of the maximum-magnitude earthquake for the source zone to as small as that of the maximum-magnitude earthquake associated with residual events. The coordinates of the source zones are given in Appendix A.

17. The Anna, Ohio seismic zone is an area of Ohio which has experienced five earthquakes in the mb range of 5.0 to 5.3 since 1875. It includes the area where the north-south trending Cincinnati arch bifurcates into the northeast trending Findlay and northwest trending Kankakee arches. Although no definite correlation between the structural features and the earthquake activity has been established, it seems possible that the arches could be responsible for locally modifying the uniform continental compressive stress field expected from plate tectonic theory, so as to cause stress concentrations and subsequently earthquakes. Table 1 lists the earthquakes in the Anna zone. The column headings are: earthquake date, origin time in Universal Time (OT), latitude (LAT) and longitude (LON) of epicenter,



Figure 3. Seismic source zones of the central United States.

Note that the boundaries of the seismic source
zones are only approximate. For sites near the
boundary of a seismic source zone independent study
must be carried out to determine if the sites
actually belong in the source zone rather than in
the surrounding, less active "Residual Events" zone,
which encompasses all of the central United States
outside of the outlined source zones

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SOURCE REGION ANNA. ON 10 AREA = 37605 KM++2

					,	AREA=	376	15 KM	**5				
	DAT		OT	(UT	,	LAT	LON	FELT	ARE	A	10	мв	MS
00	00	1845	00	00	00	41.1	84.2		0		2	3.0	
04	23	1873	04	14	00	39.7	84.2		0	3	4	3.6	
06	18	1875	13	43	00	40.2	84.0	100	-		7	5.3	
06	00	1876	00	00	00	40.4	84.2		0		0	4.2	
02	09	1882	20	00	00	40.4	84.2		250		5	4.2	
03	31	1884	19	00	00	39.5	84.7		0		2	3.0	
09	19	1884	20	14	00	40.7	84.1	320			6	4.7	
12	23	1884	23	00	00	40.4	84.2	020	0		3	3.4	
09	00	1889	00	00	00	40.4	84.2		Ö		3	3.4	
03	15	1896	07	00	00	40.3	84.2		Ö		4	3.8	
04	23	1906	07	12	00	40.7	83.6		ő		5	4.2	
00	-	1914	00	00	00	40.4			Ö		3	3.4	
-	00	1925		06	00	39.5	84.2		0		5	4.2	
03	27		04	00	00	40.4	83.9		0		3	3.4	
10	00	1925	200	00	00	40.4	84.2				3	3.4	
10	27	1928	00	12 33	200	40.4	84.1		250				
03	08	1929	09	06	00	40.4	84.2	13	000		5	4.2	
06	26	1930	21	45	00	40.5	84.0		0				
06	27	1930	07	23	00	40.5	84.0		0		4	3.8	
07	11	1930	00	15	00	40.6	83.2		0		4	3.8	
09	29	1930	21	15	00	40.4	84.2		0		3	3.4	
09	30	1930	50	40	00	40.3	84.3		0		7	5.3	
10	00	1930	00	00	00	40.4	84.2		Ú	3-	4	3.6	
03	21	1931	15	48	00	40.4	84.2		0		3	3.4	
04	01	1931	00	15	00	40.4	84.0		0			3.4	
06	10	1931	08	30	00	41.3	84.0		000		5	4.2	
09	20	1931	23	04	54	40.4	84.2	120			7	5.3	
10	08	1931	14	30	00	40.4	84.2	-	0		3	3.4	
02	23	1933	03	20	00	40.3	94.2	>	000		4	3.8	
01	31	1936	19	30	00	41.2	93.2		0		4	3.8	
01	31	1936	20	00	00	41.2	93.2		0		2	3.0	
03	02	1937	14	47	36	40.4	84.2	280			7	5.3	
03	03	1937	09	50	00	40.7	84.0		500		5	4.2	
03	03	1937	09	55	00	40.7	84.0	_	0		3	3.4	
03	09	1937	05	44	33	40.4	84.2	500		7 -	8	5.3	
04	23	1937	17	15	00	40.7	84.0		650		3	3.4	
04	27	1937	17	00	00	40.7	84.0	(650		3	3.4	
05	0.5	1937	17	05	00	40.7	94.0		0		4	3.8	
03	18	1939	00	00	00	40.4	84.0		0		2	3.0	
03	18	1939	14	03	00	40.4	84.0	1	400	3-	4	3.6	
06	18	1939	03	20	00	40.3	84.0	11	000		4	3.6	
07	09	1939	12	50	00	40.3	84.0		0		5	3.0	
11	13	1944	11	52	00	40.4	94.4	45	000		3	4.3	
04	20	1950	00	00	00	39.8	84.2	100	0		4	3.8	
01	27	1956	12	03	00	40.4	94.2		000		5	4.2	
02	22	1961	06	45	00	41.2	83.3	13	000		5	4.2	
07	26	1968	00	00	00	40.4	94.2		0	5-	3	3.2	
09	29	1974	02	26	17	41.2	83.4		0		5	3.0	

felt area in km² (a zero indicates felt area is not known), epicentral intensity (IO), body-wave magnitude (MB) and surface-wave magnitude (MS).

- 18. The North Illinois seismic zone is an area of northern Illinois and southern Wisconsin which has experienced a few moderate-sized earthquakes. The east-west trending Sandwich fault lies within the region, but there is no demonstrated relation between the fault and occurrence of earthquakes. Table 2 lists the earthquakes in the zone.
- 19. The Northern Great Plains seismic zone includes southern North Dakota, South Dakota, northern Nebraska and western Minnesota. Seismic activity is spread throughout the zone, with no apparent relation to tectonic features. The amount of earthquake activity is greater than in surrounding areas which are not assigned to a specific zone. Table 3 lists the known earthquakes which occurred within the zone.
- 20. The Nemaha Ridge seismic zone takes its name from the major north-south trending structural uplift of eastern Oklahoma, eastern Kansas and eastern Nebraska. The southern limit of the Nemaha Ridge seismic zone is indefinite. In Figure 3 it overlaps the crosstrending Wichita-Ouachita zone. Table 4 lists the known earthquakes in the Nemaha Ridge zone.
- 21. The Wichita-Ouachita source region is a zone over 1000 km long extending in an east-west direction from central Mississippi to

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SOURCE REGION NORTHERN ILLINOIS AREA = 55126 KM • • 2

1	TATE		от	(UT)	LAT	LON	FELT ARE	A 1	0 ME	MS
05	27	1881	00	0.0	00	41.3	89.1	0		4 4.7	
11	28	1907	16	30	00	42.3	89.8	250		4 3.8	
11	28	1908	00	00	00	42.2	99.8	0		4 3.8	
05	26	1909	14	42	00	42.5	89.0	800000		7 5.3	
10	22		-		00	41.8	89.7			5 4.0	
01	02			21	00	41.5	88.5	The second secon		6 4.7	
09	25	-		00	00	42.3	89.1	0	3-	4 3.6	
10	17			15	00	41.8	89.7			4 3.6	
01	23	1928	09	19	00		90.0	1000	77.	4 3.8	
12		1933				42.9	89.2			4 4.2	
11			14	45	00	41.5	90.5	-		6 4.7	
01	05		18	40	00	41.5	90.0			4 4.2	
01		1935	18	45	00	41.5	90.6			3 3.4	
11	08		05	30	00	42.5	90.7	0		3.0	
11	08	1938	07	15	00	42.5	90.7	0		3.0	
11	08	1938	09	30	00	42.5	90.7	0		0 3.0	
11	24				00	41.6	90.6			3 3.2	
03	01	1942	14	43	10	41.2	89.7	10000	4-	5 4.0	
03	16	1944	00	00	00	42.0	88.3	0		4 3.4	
03		1947	15		00		88.3			4 3.8	
09		1972					89.4	200000		6 4.4	-

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Table 3

SOURCE REGION NORTHERN GREAT PLAINS AREA = 426723 KM++2

	DATI	E	OT	(UT)	LAT	LON	FELT A	REA	10	MB	MS
02	09	1872	00	00	00	44.6	100.7		0	3	3.4	
10	09	1872	16	00	00	42.7	97.0	800	0	5	4.2	
08	17	1876	05	25	00	44.1	99.6		0	4	3.8	
11	15	1877	17	45	00	41.0	97.0	45000	0	7	5.3	
12	29	1879	06	30	00	42.9	97.3		0	5	4.0	
03	17	1884	20	00	00	41.1	100.7		0	4	3.8	
10	11	1895	23	55	00	43.9	103.3	400	0	5	4.2	
10	12	1895	01	25	00	43.9	103.3	400	0	5	4.2	
02	04	1896	11	45	00	42.6	97.3		0	3	3.4	
09	16	1898	09	59	00	42.6	97.3		0	4	3.8	
12	06	1899	12	0.0	00	44.5	99.0	1000	0	4	3.8	
07	28	1902	18	00	00	42.5	97.5	9000	0 5-	6	4.5	
12	01	1904	09	00	00	41.8	96.7		0	3	3.4	
05	10	1906	00	27	00	43.0	101.3	4500		6	4.7	
01	26	1909	20	15	00	42.3	97.8	250	0 4-	5	4.0	
02	26	1910	08	00	00	41.4	97.4		0 4-	5	4.0	
06	02	1911	22	34	00	44.2	98.2	10000	0	5	4.5	
09	16	1915	19	00	00	42.8	99.3		0 3-	4	3.6	
10	23	1915	06	05	00	43.8	101.5		0	5	4.2	
02	24	1916	04	30	00	43.0	102.5		0	3	3.4	
06	29	1916	07	45	00	43.4	99.9		0	3	3.4	
12	00	1916	00	00	00	41.5	100.5		0 2-	3	3.2	
07	14	1920	23	00	00	43.2	103.2	400	0	3	3.7	
03	16	1921	23	45	00	43.5	96.7		0 3-	4	3.6	
09	24	1921	00	30	00	43.7	98.7		0	4	3.8	
01	02	1922	14	50	00	43.8	99.3		0	6	4.7	
09	10	1923	06	30	00	41.7	96.2		0 3-	4	3.6	
12	30	1924	22	10	00	43.5	113.5	1800	0	4	3.8	
08	25	1925	06	27	00	42.8	97.4		0	4	3.8	
04	30	1927	04	15	00	46.9	102.1		0	5	3.2	
10	14	1927	16	10	00	41.6	98.9	100		4	3.8	
11	16	1928	13	45	00	44.1	103.7	500	0	5	4.2	
10	06	1929	12	30	00	42.8	97.4	180		5	4.2	
01	17	1931	18	45	00	43.7	98.7		0	4	3.8	
08	38	1933	00	0.0	00	41.9	103.7		0 4-	5	4.0	
01	29	1934	12	30	00	45.9	97.7		0	4	4.2	
05	11	1934	10	40	00	41.5	98.7	250		4	3.8	
07	30	1934	07	20	00	42.2	103.0	6000		6	4.7	
08	30	1934	03	50	00	43.4	99.1		0	4	3.6	
11	08	1934	04	45	00	42.6	100.2	300		3	3.4	
11	01	1935	10	00	00	44.0	96.6		0	3	3.4	
10	30	1936	10	30	00	43.5	103.5		0	4	3.8	
01	02	1938	17	05	00	44.5	98.2	800		5	4.0	
03	24	1938	13	11	00	42.7	103.4	500		4	3.8	
10	01	1938	22	15	00	43.8	99.3	2300		5	4.2	
10	11	1938	09	37	00	43.5	96.7	<000		5	4.2	
11	01	1938	22	10	00	43.2	28.9	500		4	3.8	
06	10	1939	18	30	00	43.0	98.9		0	4	3.8	
05	25	1941	06	25	00	43.5	103.5	5000		5	4.0	
03	11	1942	16	55	00	44.4	103.5		0 3-	4	3.6	
05	16	1943	19	40	00	43.5	173.5		0	4	3.8	

(Continued)

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MS	мв	10	A	FELT AREA	LON	LAT)	OT (UT		DATE	1
	3.8	4		0	97.9	43.0	00	09 00	1945	10	11
	4.7	6		22000	98.6	44.1	00	06 45	1946	23	07
	3.8	4		0	100.9	46.0	00	05 02	1947	14	05
	3.6	4	3-	O	100.3	44.4	00	05 45	1947	16	05
	3.8	4		0	98.9	43.1	00	14 00	1947	25	08
	3.2	3	2-	0	99.6	41.4	00	00 00	1948	07	04
	3.4	3		0	99.0	44.5	10	14 54	1949	07	05
	3.8	4		3000	99.0	42.5	00	04 15	1949	13	05
	3.8	4		0	100.0	45.0	00	00 00	1949	03	06
	3.4	3		0	99.4	43.2	00	03 15	1949	14	12
	3.8	4		0	103.5	44.1	00	00 00	1952	15	11
	3.6	4	3-	0	112.9	45.2	00	22 43	1953	21	12
	3.8	4		0	99.3	43.1	00	20 30	1953		12
	3.8	4		3000	98.6	41.3	00	01 45	1955		02
	3.8	4		250	98.2	43.8	00	07 30	1957	03	12
	3.8	4		0	98.1	44.9	00	13 00	1959	12	01
	4.5	6	5-	34000	100.3	44.4	59	16 35	1961	31	12
	3.2	3	2-	0	103.0	42.8	00	15 25	1963	09	03
	4.2	5		4000	103.5	43.5	00	06 12	1964	24	03
	4.7	7			101.7	42.8	45	10 08	1964	28	03
	3.6	0		0	101.7	42.8	50	10 24	1964	28	03
	3.8	4		0	102.2	43.8	52	16 58	1964	26	08
	3.4	0		0	96.4	44.0	00	15 41	1964	28	09
	3.5	0		0	98.6	41.4	31	09 50	1966	09	09
	3.8	5		0	99.4	43.7	39	06 23	1967	23	11
	4.4	4		25000	170.6	46.5	12	16 50	1968	08	07
	3.0	0		0	101.0	44.0	31	21 07	1971	19	10
	3.7	0		0	99.6	42.3		05 47	1972	16	10
	3.5	6		0	98.4	42.1		07 53	1975	13	05
	4.8	6		315000	96.1	45.5		14 54	1975	09	07

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Table 4

SOURCE REGION NEMAHA RIDGE AREA: 206071 KM++2

1	DATI	E	OT	(UT)	LAT	LON	FELT ARE		10	МВ	MS
04	24	1867	20	22	00	39.5	96.7	800000		7	5.3	
04	28	1867	00	00	00	40.7	95.8	0		4	3.8	
11	08	1875	10	40	00	39.3	95.5	22000		5	4.2	
12	09	1875	09	00	00	40.7	95.8	0		3	3.4	
11	15	1877	17	45	00	41.0	97.0	450000		7	5.3	
01	08	1906	00	15	00	39.3	96.6	95000	7-	8	5.5	
01	08	1906	00	38	00	39.3	96.6	0		0	3.0	
01	08	1906	04	30	00	39.3	96.6	0		0	3.0	
01	08	1906	07	00	00	39.3	96.6	0	2-	3	3.2	
01	08	1906	08	00	00	39.3	96.6	0	2-	3	3.2	
01	14	1906	15	00	00	39.3	96.6	0	2-	3	3.2	
01	16	1906	02	40	00	39.3	96.6	40000		4	3.8	
01	20	1906	05	30	00	39.3	96.6	0		3	3.4	
01	23	1906	13	40	00	39.3	96.6	0		3	3.4	
01	23	1906	14	25	00	39.3	96.6	0		3	3.4	
01	11	1907	07	45	00	37.1	97.0	0		4	3.8	
07	19	1908	00	00	00	35.7	97.7	0		3	3.4	
09	10	1918	16	30	00	35.5	98.0	1000	5-	6	4.5	
09	11	1918	06	30	00	35.5	97.9	1000	5-	6	4.5	
09	11	1918	09	00	00	35.5	97.9	0	2-	3	3.2	
00	00	1918	00	0.0	00	35.5	97.7	0	3-	4	3.6	
05	27	1919	03	06	00	37.7	97.3	25000		4	4.2	
07	26	1919	10	00	00	37.7	97.3	0		3	3.4	
07	26	1919	12	55	00	37.7	97.3	10000		4	3.8	
06	03	1924	00	40	00	36.3	96.5	0		3	3.4	
01	07	1927	09	30	00	38.3	97.7	10000		5	4.2	
09	23	1929	10	00	00	39.0	96.6	U		5	4.0	
09	23	1929	11	00	00	39.0	96.6	40000		5	4.2	
10	21	1929	21	30	00	39.2	96.5	20000		5	4.2	
10	23	1929	00	00	00	39.0	96.8	0	2-	3	3.2	
12	07	1929	09	05	00	39.2	96.6	2500		5	4.2	
12	28	1929	0.0	30	00	35.5	97.9	17000		6	4.7	
08	19	1933	19	30	00	35.5	98.0	500		6	4.7	
03	01	1935	10	59	44	40.3	96.2	210000		7	5.3	
03	01	1935	11	04	00	40.3	96.2	0		0	3.0	
03	22	1935	22	45	00	40.3	96.1	0		4	3.8	
06	08	1937	14	26	00	35.3	96.9	2500		4	3.8	
10	18	1941	07	48	00	35.4	99.0	250		5	4.2	
06	12	1942	04	50	00	36.4	97.9	4000		3	3.4	
04	03	1948	03	00	00	37.7	97.3	0		4	3.8	
04	09	1952	16	29	29	35.4	97.8	640000		7	5.5	
04	11	1952	18	30	00	35.4	97.8	0	2-	3	3.2	
04	11	1952	20	30	00	35.4	97.8	8000		4	3.8	
04	16	1952	05	58	00	35.4	97.8	8000	2-	3	3.2	
04	16	1952	06	05	00	35.4	97.8	8000		5	4.2	
07	17	1952	00	30	00	35.4	97.8	0	3-	4	3.6	
07	17	1952	02	00	00	35.4	97.8	0	3-	4	3.6	
08	14	1952	21	40	00	35,4	97.8	0		4	3.8	
03	16	1953	12	50	00	35.4	97.9	0		3	3.4	
03	17	1953	13	12	00	35.6	96.0	0		5	4.2	
03	17	1953	14	25	00	35.6	98.0	7000		6	4.7	

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Table 4 (Concluded)

1	DAT	E	OT	(UT)	LAT	LON	FELT AREA	10	MB	MS
01	06	1956	11	57	59	37.3	98.7	00000	6	4.7	
02	16	1956	23	30	00	35.4	97.3	13000	6	4.7	
06	17	1959	10	27	07	34.6	98.4	37000	6	4.7	
10	10	1965	23	51	33	36.1	97.7	0	0	3.1	
05	30	1969	14	08	05	34.8	97.8	0	0	3.0	
07	01	1969	03	36	58	37.4	97.0	0	0	3.0	
09	13	1975	01	25	03	34.1	97.4	0	4	3.8	

the panhandle of Texas. Earthquakes in this zone for which focal mechanisms solutions could be obtained have fault planes which strike along the direction of the mountain front. Table 5 lists the earthquakes associated with this zone.

- 22. The Wabash Valley seismic zone includes southeastern Illinois and western Indiana. Five earthquakes with $m_{\tilde{b}}$ greater than or equal to 5 occurred within it in the last 100 years. Many of the earthquakes apparently are related to the approximately north-south trending Wabash valley fault zone. Table 6 contains the earthquakes of that region.
- 23. The Ozark Uplift zone includes the St. Francois highlands of southeast Missouri and the Illinois basin of southwestern Illinois. It also contains the Centralia, Illinois fault zone, near which there were several damaging earthquakes in the nineteenth century. Table 7 contains the earthquakes located in the Ozark Uplift zone.
- 24. The New Madrid seismic zone is by far the most active region of the central United States, even if one considers only the earthquakes which happened after 1812. For this report the zone is subdivided into regions A and B, the former being the central area with the higher rate of seismicity and linear microearthquake trends (Figure 1) and the latter the surrounding area. Table 8 and 9 list the earthquakes located in each of the two regions.
- 25. The Residual Events zone includes all of the central United States which does not lie in one of the previously described source

SOURCE REGION WICHITA-OUACHITA AREA: 261829 KM++2

	DATE		OT	(UT)	LAT	LON	FELT AR	E 10	MB	MS
07	18	1894	00	00	00	35.0	90.0	0			
01	27	1898	01	35	00	34.6	90.6	Ö			
04	00	1907	00	00	00	35.5	101.2	0			
07	19	1908	00	00	00	35.7	97.7	Ö			
03	31	1911	16	57	00	33.8	92.2	50000			
03	31	1911	18	10	00	33.8	92.2	6500			
10	08	1915	16	50	00	35.7	95.3	8000			
01	28	1917	00	00	00	3.4	101.3	0			
03	24	1917	00	00	00	35.3	101.2	ō			
03	27	1917	19	56	03	35.3	101.3	5000			
03	27	1917	23	38	00	35.3	101.3	0			
09	10	1918	16	30	00	35.5	98.0	1000			
09	11	1918	06	30	00	35.5	97.9	1000			
09	11	1918	09	00	00	35.5	97.9	0			
10	04	1918	09	21	00	34.7	91.7	80000			
00	00	1918	00	00	00	35.5	97.7	0			
07	30	1925	12	17	00	35,4	101.3	500000	_		
01	20	1926	00	00	00	35.6	94.9	47000			
06	20	1926	14	20	00	35.6	94.9	47000			
12	28	1929	00	30	00	35.5	97.9	17000			
10	16	1930	12	30	00	34.3	92.7	0			
11	16	1930	12	30	00	34.3	92.8	900			
08	19	1933	19	30	00	35.5	98.0	500			
04	11	1934	17	40	00	33.9	95.5	8000			
03	14	1936	17	20	00	34.0	95.2	2300			
06	20	1936	03	13	00	35.7	101.4	0			
06	20	1936	03	18	00	35.7	101.4	0			
06	20	1936	03	24	06	35.7	101.4	110000			
07	12	1936	00	23	00	36.9	102.9	506			
86	08	1937	14	26	00	35.3	96.9	2500			
04	26	1938	05	42	00	34.2	93.5	0			
06	01	1939	07	30	00	35.0	96.4	65000	4		
06	19	1939	21	43	12	34.1	92.6	65000			
10	18	1941	07	48	00	35.4	99.0	250			
03	12	1948	04	29	00	36.0	102.5	300000			
06	20	1951	19	37	10	35.0	102.0	65000			
04	09	1952	16	29	29	35.4	97.8	640000	7		
04	11	1952	18	30	00	35.4	97.8	0	2- 3	3,2	
04	16	1952	20	30	00	35.4	97.8	8000		3.8	
04	16	1952	05	58	00	35.4	97.8	8000			
04	16	1952	06	05	00	35.4	97.8	8000	5	4.2	
07	17	1952	00	30	00	35.4	97.8	0	3- 4	3.6	
07	17	1952	02	00	00	35.4	97.8	0			
08	14	1992	21	40	00	35.4	97.8	0			
10	80	1952	04	15	00	35.1	96.5	0		3.8	
03	16	1953	12	50	00	35,4	97.9	0		3.4	
03	17	1953	13	12	00	35.6	98.0	0		4.2	
03	17	1953	14	25	00	35.6	98.0	7000	6		
06	06	1953	17	40	00	34.7	96.7	0			
04	11	1954	00	00	00	35.0	96.4	0	4		
04	12	1954	23	05	00	35.0	96.4	0	4	3.8	

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Table 5 (Concluded)

M	MD	0		ARE	FELT	LON	LAT)	TU	OT		TATE	1
	3.8	4		0		96.4	35.1	00	48	18	1954		04
	4.7	6		00	130	97.3	35.4	00	30	23	1956	16	02
	4.2	5		00		95.6	34.2	00	03	16	1956	02	04
	4.5	5		00	1200	100.9	35.5	00	05	20	1999	10	12
	4.2	5		00	130	96.7	34.7	00	45	12	1959	15	06
	4.7	6		00	370	98.4	34.6	07	27	10	1959	17	16
	3.8	4		0		92.0	34.2	32	31	16	1960	04	15
	4.2	5		00	65	95.5	34.9	00	40	01	1961	11	1
	3.8	3		00	65	95.0	34.6	00	05	07	1961	26	04
	3.0	0		0		95.0	34.6	00	00	03	1961	27	14
	3.0	0		0		95.0	34.6	00	00	05	1961	27	14
	4.2	5		00	200	95.3	34.9	00	30	07	1961	27	14
	3.4	0		0		92.1	34.4	36	18	21	1963	07	12
	4.2	5		0		99.7	35.1	00	23	08	1964	02	2
	3.1	0		0		97.7	36,1	33	51	23	1965	10	0
	3.8	5	4-	00	300	101.4	35.6	59	04	09	1966	20	7
3.	4.5	6		00	540	90.9	33.6	14	14	16	1967	04	6
	4.0	5		0		90.9	33.6	07	57	13	1967	29	6
	3.8	4		0		95.5	34.9	00	00	00	1968	04	1
3.	4.5	6		00	620	92.6	34.8	36	35	23	1969	01	1
	3.5	0		0		96.3	34.2	51	27	06	1969	13	14
	4.0	5		0		96.3	35.2	20	33	11	1969	02	15
	3.0	0		0		97.8	34,8	05	08	14	1969	30)5
	3.5	3		0		90.6	33.8	37	11	09	1973	08	1
	3.4	3		0		90.8	33.9	14	40	14	1973	25	15
	3.2	0		0		90.8	33.9	32	42	14	1973	25	14
	4.6	5		0		100.7	36.5	49	33	13	1974	15	12
	3.6	3		0		93.1	33.9	35	32	22	1974	15	12
	3.6	3		0		93.1	34.0	45	35	22	1974	15	12
	4.0	5		0		93.0	34.0	02	49	22	1974	15	12
	3.4	5		0		91.9	34.7	58	03	05	1974	13	2
	3.0	3	2-	0		90.9	34.9	00	19	09	1975	02	1

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Table 6 FROM COPY FURNISHED TO DDC

SOURCE REGION HABASH VALLEY AREA= 39780 KM++2

					AKEA=	397		• * 2				
-	DATE	0	TOT	,	LAT	LON	FELT	ARE	A :	10	MB	MS
08	07 18				37.8	87.5	80	000		5	4.4	
03	26 18			00	37.1	88.6		0		3	3.4	
09	25 18			00	38.5	87.8		0		6	4.7	
09	25 18			00	38.5	87.8	150			6	4.7	
09	26 18			00	38,5	87.8		0		3	3.4	
05	26 18			00	38.2	87.9		ŏ	3-	4	3.6	
1000	10 18		-	00	37.4	89.3		Ö	3-	3	3.4	
01	06 18				38.7	87.5	170		5-	6	4.7	
07	27 18				37.9	87.5	1,0	000	,-	6	4.5	
04					38.8	87.0	100	-	6-	7	5.0	
22 12					30.8	87.0	100	0	0-	4	3.8	
09	21 19			00	38.7	88.1		200		4	3.8	
05	11 19				38.5	87.2				4	3.8	
09	07 19			00	38.2	87.7	1	500		5		
01	30 19				39.5	86.6	250	0		7	4.2 5.3	
09	27 19			00	37.5	87.4				5	4.2	
10	23 19			00	39.0	87.8		000				
02	05 19			00	37.7	88.6		000	•	4	3.8	
04	15 19			00	38.7	88.1		000	2-	3	3.8	
01	07 19			00	39.1	87.0		000		3	3.8	
02	18 19			00	37.6	88.8		0		3		
02	11 19			00	37.8	87.5		000	3-		3.8	
05	25 19			00	38.4	87.5		000		5	4.4	
03	14 19			00	39.5	87.5	05	000		4	4.4	
03	31 19			00	37.9	87.8		0			3.8	
10	01 19			00	37.7	88.6		000		4	4.0	
01	11 19			00	37.9	87.8		000	4-	5	4.2	
03	22 19			00	37.3	88.9	150			5	4.6	
03	23 19			00	37.3	88.9		0		5	4.2	
11	27 19			00	37.8	88.5	130	-	6-	7	5.0	
04	02 19			00	37.1	88.6		0		4	3.8	
04	27 19			00	38.3	87.6	250	-	6-	7	5.0	
09	02 19		_	00	37.8	87.5	200	-		6	4.8	
09	20 19			00	37.8	87.5		000		4	4.1	
03	22 19			00	37.8	88.6	10	000		4	4.0	
10	04 19			00	38.3	87.6		0		3	3.4	
10	27 19			00	38.3	87.6		000		4	4.0	
01	14 19			00	38.3	87.6		500		4	3.8	
01	06 19			00	39.0	87.0		300		5	4.2	
04	01 19			09	36.9	88.3	- 5	000		3	3.8	
12	31 19			00	38.5	87.2		0		2	3.0	
10	30 19			47	37.5	88.5		000		4	3.8	
05	31 19			00	37.1	88.6		500		5	4.2	
12	29 19			00	37.9	87.3		800		3	3,6	
03	29 19			00	37.7	88.6		500		4	3.8	
03	26 19			00	37,0	88.4		0		4	4.0	
08	09 19			00	38.5	87.3		0		4	3.8	
04	11 19			00	37.7	88.6		0		2	3.0	
05	30 19		1000	00	38 1	88.9		0		3	3.4	
03	26 19			06	37.0	88.4		800		4	3.8	
11	08 19			43	38.4	87.9		000		6	4.7	
06	27 19	62 01	28	56	37.7	88.5	45	000		5	4.4	

(Continued)

THIS PAGE IS BEST QUALITY PRACTICABLE FROM COPY FURNISHED TO DDC Table 6 (Concluded)

MS	MB	10	FELT AREA	LON	LAT	OT(UT)			DATE		
	3.1	0	0	88.2					1966		
5.2	5.5	7	1600000	88.5	38.0	41	01	17	1968	09	11
	3.8	4	0	88.5	38.0	17	08	17	1968	09	11
	3.2	0	0	88.9	37.9	13	10	13	1969	28	02
	3.0	0	0	89.0	38.0	00	16	23	1970	08	12
	3.3	4	10000	87.9	38.5	27	44	12	1971	12	02
	4.7		0	88.1	38.6	02	05	23	1974	03	04

Table 7

SOURCE REGION OZARK BPLIFT AREA: 36557 KM++2

						WEY-	3022	, MM	•••				
	DAT		OT	CUT	,	LAT	LON	FELT	ARE		10	MB	MS
09	02	1819	08	00	00	37.7	89.7		0		5	4.2	8.0
09	17	1819	04	00	00	38.1	89.8		ō		4	3,8	0.0
09	17	1819	00	00	00	38.1	89.8		0	3-	4	3.6	8.0
06	. 09	1838	14	45	00	38,5	89.0	500	-	7-	8	5.7	0.0
10	08	1857	10	00	00	38.7	89.2	200		, -	7	5,3	
07	24	1871	00	00	00	37.0	90.0	200	0		3	3.4	
07	25	1871	06	40	00	38.5	90.0	21	500		3	3.6	
07	28	1882	00	00	00	37.6	90.6		000	3-	4	4.1	
09	27	1882	10	20	00	39.0	89.5	100		3-	4	4.7	
10	15	1882	05	50	00	39.0	89.5		000		5	4.2	
10	15	1882	10	35	00	39.0	89.5		000		5	4.2	
10	22	1882	06	10	00	38.9	89.4	- 01	0		3	3.4	
12	05	1883	15	20	00	36.3	91.2	2501			5	3.4	
02	14	1884	12	00	00	37.7	90.7	2001	0		5 3 3 3	3.4	
10	30	1895	14	30	00	36.4	90.6		ŏ		3	3.4	
10	30	1895	20	00	00	36.4	90.6		Ö		3	3.4	
10	30	1895	22	30	00	36.4	90.6		Ö		3	3.4	
04	15	1898	03	20	00	36.4	90.6		Ö		0	3.0	
02	09	1903	00	21	00	37.8	89.3	180	7		6	4.8	
20	05	1903	02	56	00	37.0	90.0	120		5-	6	4.6	
11	03	1903	18	00	00	37.8	89.3	120	0	3-	4	3.6	
01	30	1907	00	00	00	38.9	09.5	7		3-	5	4.2	
07	04	1907	09	00	00	37.8	89.5		000	4-	5	3.8	
08	16	1909	22	45	00	38.3	90.1		000	-	4	4.3	
10	22	1909	22	00	00	37.6	90.6	73	0		4	3.8	
04	09	1917	20	52	00	38.1	90.2	550			6	5.0	
04	09	1917	23	38	00	38.1	90.2		0		4	3.8	
05	08	1917	09	00	00	36.8	90.4	10	000	3-	4	3.9	
05	08	1917	15	00	00	36.8	90.4		0		3	3.4	
06	09	1917	13	14	00	36.8	90.4	45	000		4	4.3	
10	13	1918	09	30	00	36.1	91.0		500		5	4.2	
04	08	1919	12	30	00	36.2	91.3		0	3-	4	3.6	
11	03	1919	20	40	00	36.3	91.0		0	4-	5	4.0	
04	30	1920	15	12	00	38.6	89.1	100	000		4	4.0	
05	01	1920	15	15	00	38.5	89.5		000	4-	5	4.3	
05	01	1920	16	09	00	38,5	89.5		0		0	3.0	
09	09	1921	03	00	00	38.3	90.1	10	000		4	4.0	
09	09	1921	05	45	00	38.3	90.1		. 0		0	3.0	
10	09	1921	07	50	00	38.3	90.1	8	000		3	3.8	
10	09	1921	11	50	00	38,3	90.1		0		3	3.4	
03	28	1922	16	42	00	36.7	90.4	61	000		3	4.0	
03	09	1923	04	45	00	38.9	89.4		000	3-	4	3.9	
02	01	1927	01	30	00	37.4	89.7		000		4	4.0	
02	02	1927	08	00	00	36.7	90.4		000		4	3.8	
11	10	1928	06	20	00	36.1	91.1		0		4	3.8	
12	26	1928	03	25	00	36.1	91.1		0		4	3.8	
02	26	1929	08	15	00	37.6	90.6		0		4	3.8	
01	26	1930	21	00	00	36.1	91.1		0		4	3.6	
02	25	1930	12	45	00	37.0	90.2		0	3-	4	3.6	
03	11	1933	12	48	00	36.7	90.4		0		4	3.8	
03	11	1933	13	04	00	36.7	90.4		0		4	3.8	

(Continued)

M	MB	0	,	REA	AF	7	FELT	LON	LAT)	CUT	OT		TAC	1
	3.4	3	,	0		'		89.9	37.9	39	42	14		13	7
	3.8	4			200				77.0	15	34	04	1933	04	8
						1 2	,	89.9	37.9		53			-	
	3.4	3	_	0				89.9	37.9	00		13	1934	17	4
	3.6	4	3-					89.9	37.9	00	28	14	1934	15	5
	3.0	2		0				90.6	36.6	40	38	09	1936	23	1
	3.0	2		0				90.6	36.6	35	42	17	1936	25	1
	3.2	3	2 -	0	0			89.9	37.7	00	58	11	1937	18	2
	4.4	5		00	000	00	50	89.1	38.6	00	04	17	1937	17	1
	3.4	3		0	0			89.9	37.7	00	18	04	1938	17	1
	4.9	5		0.0	000	00	400	90.1	38.2	53	14	15	1939	23	1
	3.4	3		0		-		90.2	38.3	00	04	20	1941	15	1
	3.8	4			300	23	2	89.7	37.5	00	18	05	1944	07	1
	4.4	4			000			90.0	37.9	23	37	11	1944	25	è
	3.8	4		1000	800	-300		90.2	37.8	00	00	04	1945	16	1
	3.8	4							38.6	00	52	00	1946	25	2
					000			89.1							
	4.2	4	3-		000			90.8	36.6	00	10	06	1946	15	5
	4.4	5	4-		000			90.6	37.5	02	12	01	1946	08	0
	4.2	4			000		27	90.6	36.7	33	47	07	1947	01	2
	4.0	5	4-	0	000	£		89.1	38.6	00	34	01	1948	06	1
	3.4	3		0	00	8		90.3	38.1	36	51	19	1949	08	6
	3.8	4		0	000	30	3	89.1	38.6	00	00	22	1953	30	2
	4.4	6		0	000	00	80	90.3	36.7	00	53	16	1954	02	2
	4.5	6	5-	0	000	00	50	89.9	38.1	24	01	13	1955	09	4
	4.7	6		0	000	00	70	90.6	37.1	44	12	04	1956	26	1
	3.8	4		0	0	-		91.3	36.4	02	43	22	1961	09	9
	3.1	0		0	0			90.5	37.0	43	51	23	1963	08	7
	3.0	0		o				91.1	37.1	34	09	08	1964	24	9
4	4.9	6		-	_	00	420	91.0	37.5	38	04	02	1965	21	Ó
•••	3.0	0		0			7-0	91.1	37.1	22	33	12	1965	03	1
	3.5	0		ŏ				91.1	37.1	39	43	07	1965	04	i
	3.1			Ö					77.1	56	08	00	1966	14	
		0						90.9	37.2						2
	3.7	0		0				91.0	37.2	20	10	80	1966	26	2
2.8	4.3				000	3 D	23	90.4	37.5	49	14	09	1967	21	7
	3.1	0		0				91.1	37.1	18	15	19	1967	25	
	3.6	4		0				91.0	37.1	37	19	23	1966	13	2
	3.4	3		0	0			90.4	37.8	00	25	19	1969	20	1
	3.0	0		0	0			89.0	38.0	00	16	23	1970	08	2
2.1	4.2	6	5 -	0	00	70	27	90.8	36.4	10	42	05	1972	01	2
	3.1	4	3-		50		-	90.4	37.7	19	15	19	1972	09	•
	3,2	4	•	0		9		90.5	37.9	56	56	11	1973	12	1
	3.6			Ö				89.9	38.6	11	06	08	1974	05	i
	3.6	5		0				91.2	36.9	45	29	14	1974	11	8

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Table 8 FROM COPY FURNISHED TO DDC

SOURCE REGION NEW MADRID A AREA = 22506 KM4+2

						AREA	223	00 K	M	4			
-	TATE		OT	(UT)	LAT	LON	FEL	TA	REA	10	MB	MS
12	16	1811	08	15	00	36.0	90.0	500			-11	7.2	8.0
01	23	1812	15	00	00	36.3	89.6	500			-11	7.1	7.8
02	07	1812	09	45	00	36.5	89.6	500			-12	7.4	8.2
07	25	1816	15	00	00	36.5	89.5				- 4	3.6	8.0
07	25	1816	21	00	00	36.5	89.5			0 3		3.6	0.0
03	00	1818				36.2	89.7			0	3	3.4	
		1820				36.6	89.5			0 3	- 4	3.6	
12	28	1841	05	50	00	36.6	89.2			0	5	4.2	0.0
05	28	1842	05	00	00	36.6	89.2			0	4	3.8	0.0
11	04	1842	06	30	00	36.6	89.2			0	5	4.2	
11	04	1842	08	30	00	36.6	89.2			0	5	4.2	
01	05	1843	02	45	00	35.5	90.5	150			8	6.0	
02	17	1843	05	00	00	35.5	90.5	25	000		5	4.8	
06	13	1843	15	00	00	36.6	89.2			0	3	3.4	
03	26	1846	17	25	00	36.6	89.6			0	5	3.4	
08	28	1853	00	00	00	36.6	89.2				3	3.4	
12	12	1853	00	00	00	36.6	89.2	10	000		- 5	4.5	
11	09	1856	00	00	00	36.6	89.5		000		4	4.4	
02	00	1857	00	00	00	36,6	89.5	•			4	3.8	
09	21	1858	00	00	00	36.5	89.2			0	6	4.7	
08	17	1865	15	00	00	36.5	89.5	25	000		7	5.3	
09	07	1865	14	15	00	36.6	89.5			3	4	3.6	
11	21	1868	00	00	00	36.6	89.2		-	0	3	3.4	
12	14	1870	00	00	00	36.6	89.2		-	3		3.6	
04	20	1872	07	00	00		90.0			0	3	3.4	
08	20	1872	00	00	00	35.1	90.0			0 2		3.2	
05	03	1873	21	00	00	36.6	89.6	3	000		4	4.2	
0.8	22	1873	19	00	00	35.1	90.0	-		2		3.2	
10	07	1875	00	00	00	36,1	89.6	יכ	000			4.3	
10	28	1875	03	00	00	35.1	90.0	41		3	4	3.8	
03	15 12	1878	10	00	00	36.8	89.7		500		- 4	4.3	
11	19	1878	05	52	00	36.8	89.3		000		4	4.9	
09	26	1879	03	10	00	35.3	90.3		000			3.9	
07	14	1880	02	30	00	35,3	90.3		500		4	4.1	
10	07	1881	16	52	00	35.1	90.0	-	-		4	3.8	
06	11	1883	18	16	00	35.1	90.0				4	4.7	
11	30	1884	05	00	00	35,5	89.7	1	200		4	4.0	
11	03	1888	00	00	00	35.4	90.4)	4	3.8	
06	06	1889	04	28	00	35.1	90.0		()	3	3.4	
07	20	1889	01	32	00	35.2	90.0)	6	3.8	
01	14	1891	00	00	00	35.1	90.0			3		3.6	
01	14	1892	09	05	00	35.1	90.0				3	3.4	
07	18	1894	00	00	00	35.0	90.0				3	3.4	
10	03	1895	00	00	00	35.2	90.0				3	3.4	
10	18	1895	03	10	00	36.6	89.5				3	3.4	
04	18	1897	04	00	00	36.6	89.5	21	000		- 5	4.1	
06	14	1898	15	20	00	36.0	89.6		0000		- 4	4.5	
02	15	1901	00	15	00	36.0	90.0		000		4	4.2	
02	-	7407			• 0	00.0	, u . u	3(-	41.5	

(Continued)

(Sheet 1 of 5)

Table 8 (Continued)

1	TAC		OT	IUT)	LAT	LON	FELT A	REA	10	MB	MS
09	14	1901	00	00	00	35.1	90.0		0	3	3.4	
11	04	1903	18	18	00	36.9	89.3	34000		7	5.3	
11	04	1963	19	14	00	36.9	89.3	34000	o	6	4.7	
11	24	1903	15	20	00	36.6			Ö	3	3.4	
					200	30.0	89.5			3		
11	25	1903	00	00	00	36.6	89.5		0 2-		3.2	
11	27	1903	07	00	00	36.5	89.5	3000		5	4.2	
11	27	1903	00	20	00	36.5	89.5	18000	-	5	4.2	
08	22	1905	05	08	00	36.8	89.6	32500		7	5.0	
09	28	1908	19	34	00	36.6	89.6	1300		4	4.0	
10	23	1909	07	10	00	37.0	89.5	12500	0 5-	6	4.6	
04	28	1915	23	40	0	36.5	89.5	50	0 4-	5	4.0	
12	07	1915	18	40	00	36.7	89.1	12000	0 5-	6	4.6	
05	21	1916	18	24	00	36.6	89.5	2000	0	4	4.1	
12	19	1916	05	42	00	36.6	89.2		0 5-	6	4.5	
05	23	1919	12	30	00	36.6	89.2	800	0	3	3.9	
05	24	1919	13	30	00	36.6	89.2	800		3	3.9	
05	26	1919	13	25	00	36.6	89.2	800		3	3.8	
05	28	1919	11	30	00	36.6	89.2	800	7.	3	3.8	
05	28	1919	13	45	00	36.6	89.5	800		3	3.8	
01	09	1921	21	54	00	36.4	89.5	500		4	3.8	
03	30	1922	16	53	00	36.1	89.6	4000		5	4.2	
10	28	1923	17	10	00	35.5	90.4	12000		7	5.3	
-	26	1923	23	25	0.0	35.5	90.4	2300		4	4.1	
11		1924	03	05	00	35.4		15000		5	4.6	
01	01	1924	05	42	00	36.4	90.3			5	4.2	
06	07 28	1926	04	16	00	36.2	89.5	2500 1000		4	4.0	
				03	00		89.6					
12	13	1926	23	00	00	36.7	89.4	800		3	3.8	
12	17	1926				36.4	89.5	1000		4		
04	18	1927	10	30	00	36,3	89.5	1000			4.0	
05	07	1927	08	28	00	35.7	90.6	30000		7	5.3	
0.8	13	1927	16	10	00	36.4	89.5	6500		5	4.4	
04	15	1928	11	00	00	36.6	89.5		0	4	3.8	
04	23	1928	11	00	00	36.5	89.2		0	4	3.8	
05	31	1928	22	40	00	36.6	89.5		0	4	3.8	
05	13	1929	03	50	00	36.4	89.5	500		3	3.8	
01	02	1930	16	30	00	35.7	89.5		0	5	3.0	
02	18	1930	17	00	00	35.5	90.4		0	3	3.4	
03	26	1930	08	50	00	35.2	89.9		0 5-	3	3.2	
03	27	1930	08	56	00	35.1	90.1	100		4	3.8	
04	0.5	1930	09	39	00	36.1	89.7		0	4	3.8	
08	13	1930	19	59	52	36.6	89.5		0	2	3.0	
09	01	1930	20	27	28	36.6	89.4	1000	0	5	4.2	
07	18	1931	14	52	00	36.6	89,5	500	0	4	3.8	
12	10	1931	08	11	36	35,9	89.9	500	0	4	3.8	
11	22	1931	07	56	42	36.0	90.2	250	0	3	3.6	
12	09	1933	08	50	00	35.8	90.2	25	0	6	4.2	
07	02	1934	15	10	41	35.2	90.0		0	4	3.8	
07	03	1934	00	00	00	36.2	89.7		0	2	3.0	
07	24	1935	01	38	00	36.4	89.5		0	4	3.8	
02	17	1936	05	05	08	36.2	89.7		0	4	3.8	
08	02	1936	22	16	25	36.7	89.0	2000	0	3	3.8	

(Continued)

(Sheet 2 of 5)

THIS PAGE IS BEST QUALITY PRACTICABLE FROM COPY FURNISHED TO DDQ

Table 8 (Continued)

			-										
1	DATE	•		(UT		LAT	LON	FELT	ARE		10	MB	MS
10	20	1936	21	17	00	36.6	89.6		0		2	3.0	
10	31	1936	16	11	38	36.6	89.6		0		2	3.0	
01	30	1937	08	57	09	36.2	89.7	51	000		4	3.8	
06	23	1937	15	28	00	36.4	89.5		0		3	3.4	
10	05	1937	22	58	00	36.6	89.5		0		3	3.4	
03	16	1938	10	12	00	36.6	89.6		0		2	3.0	
06	17	1938	00	00	00	35.8	89.9		0		3	3.4	
09	17	1938	01	57	00	35.5	90.3		0		0	3.0	
09	17	1938	03	34	24	35.5 35.5	90.3	250		4-	5	4.8	
09	17	1938	07	20	00	35.5	90.3		0	2-	3	3.2	
09	28	1938	11	35	00	36.5	89.9		0		3	3.4	
04	15	1939	17	25	00	36.8	89.4	11	000		3	3.4	
09	19	1939	00	00	00	36.4	89.5		0		3	3.4	
02	14	1940	11	10	00	35.9	89.8		0		3	3.4	
09	19	1940	23	43	00	36,5	89.6		0	2-	3	3.2	
10	10	1940	19	34	00	36.8	89.2		0	2-	3	3.2	
10	08	1941	07	51	00	36.2	89.7	3	000	4-	5	4.0	
08	27	1941	03	59	00	36.7	89.7		0		3	3.4	
11	15	1941	03	07	00	35.1	90.0		0		4	3.8	
11	17	1941	03	08	00	35.5	89.7	501	000		6	4.7	
11	30	1942	16	53	00	36.8	89.7		0		3	3.4	
12	23	1944	07	23	00	36.2	89.7		0		4	3.8	
05	02	1945	11	23	00	36.5	89.7	51	000		4	3.8	
08	06	1945	23	52	00	36.1	89.7		0		3	3,4	
08	07	1945	04	05	00	36.1	89.7		0		3	3.4	
09	23	1945	06	23	00	36.0	89.8		0		4	3.8	
10	27	1945	10	42	00	36.5	89.5		0		3	3.4	
12	15	1947	03	27	00	35.6	90.1		000		5	4.2	
01	14	1949	03	49	00	36.4	89.7		000		5	4.2	
01	31	1949	00	00	00	36.3	89.7	41	000		5	4.2	
08	13	1949	21	45	00	36.1	89.7		0		3	3.4	
05	01	1950	15	30	00	36.5	89.9		0	2-	3	3.2	
09	17	1950	05	48	00	35.7	89.9		0	3-	4	3.8	
12	18	1951	02	05	00	35.6	90.3		0		3	3.4	
12	18	1951	08	00	00	35.6	90.3		0	2-	3	3.2	
02	20	1952	22	34	39	36.4	89.5	341	000		5	4.2	
03	17	1952	01	30	00	36.2	89.6		0		4	3.8	
05	28	1952	09	54	14	36.6	89.7	3 (000		4	3.8	
07	16	1952	23	48	10	36.2	89.6		0		6	4.7	
07	17	1952	00	09	00	36.2	89.6		0		4	3.8	
10	17	1952	04	16	00	36.2	89.6	11	000		4	3.8	
10	17	1952	04	30	00	36.2	89.6		0	2-	3	3.2	
10	17	1952	04	35	00	36.2	89.6		0	5-	3	3.2	
10	17	1952	04	46	00	36.2	89.6		0	2-		3.2	
12	25	1952	04	23	24	35,9	89.8	231	000		4	4.1	
12	25	1952	00	00	00	35,9	89.8		0		2	3.0	
12	28	1952	16	59	00	36.7	89.6		0		3	3.4	
01	26	1953	23	18	00	36.0	89.5		0		4	3.8	
01	27	1953	06	48	00	36.0	89.5		0		4	3,8	
01	27	1953	07	48	00	36.0	89.5		0		2	3.0	
02	11	1953	10	50	54	36,5	89.5	30	000		4	3,8	

(Continued)

(Sheet 3 of 5)

Table 8 (Continued)

	DAT	E	OT	(UT)	LAT	LON	FELT	AREA	10	мв	MS
02	17	1953	11	05	00	36.5	89.5		0	4	3.6	
02	18	1953	00	17	00	36.5	89.5		Ö	3	3.4	
02	19	1993	05	05	00	36.0	89.5		ŏ	3	3.4	
05	12	1953	18	50	00	35.6	90.3		Ö	4	3.8	
				-						4		
01	17	1954	07	15	00	36.0	89.4		000		3.8	
04	27	1954	04	09	00	35.1	90.0	400		5	4.4	
01	25	1955	07	24	30	36.0	89.5	900		6	4.7	
03	59	1955	09	03	00	36.0	89.5	100		6	4.7	
09	06	1955	01	45	00	36.0	89.5		0	5	4.2	
09	06	1955	00	00	00	36.0	89.5		0	3	3.4	
09	24	1955	18	45	00	36.4	89.5		0	4	3.8	
12	13	1955	07	43	00	36.0	89.5		0	5	4.2	
12	13	1955	07	56	00	36.0	89.5		0	3	3.4	
01	24	1956	05	00	00	36.1	89.7		0	2- 3	3.2	
01	29	1956	04	44	15	35.6	89.6	130		6	4.7	
10	29	1956	09	23	44	36.1	89.7		0	5	4.2	
08	17	1957	23	00	00	36.2	89.5		0	4	3.8	
01	26	1958	16	55	37	36.1	89.7	170		5	4.2	
04	08	1958	22	25	33	36.3	89.2		00	5	4.2	
04	26	1958	07	30	00	36.4	89.5		300	4	4.2	
05	20	1958	01	25	00	35.5	90.4	1.	0	4	3.8	
01	21	1959	15	35	00	36.3				4	3.8	
02		1959	08	37	00	36.1	89.5		0	5	4.2	
	13		08	15	26	35.9	89.5		150	3		
07	20	1959		25	00	36.0	89.8		0	5	4.2	
12	21	1959	16	38	00	30.0	89.5		00	5		
01	28		21	45		36.0	89.5		00		4.2	
04	21	1960	10	43	29	36.0	89.5	0.00	0	5	4.2	
02	02	1962	06			35.6	89.6	900		6	4.3	3.5
06	01	1962	11	23	41	36.0	90.2		0	0	3.2	
07	23	1962	06	05	18	36.1	89.8	100		6	4.2	
03	31	1963	13	31	04	36.5	89.5		0	0	3.0	
04	06	1963	08	12	24	36.4	89.8		0	0	3.1	
05	02	1963	01	09	22	36.7	89.4		0	0	3.1	
01	16	1964	05	0.9	57	36.8	89.5		0	0	3.2	
01	25	1964	19	54	10	36.5	89.5		0	0	3.0	
03	17	1964	02	16	06	36.2	89.6		0	0	3.5	
05	23	1964	11	25	34	36.5	89.9		0	0	3.9	
05	23	1964	15	00	35	36.5	90.0		0	0	3.6	
02	11	1965	03	40	24	36.4	89.7		0	3	3.3	
03	25	1965	12	59	28	36,4	89.5		0	0	3.7	
05	25	1965	07	15	43	36.1	89.9		0	0	3.3	
06	01	1965	07	24	57	36.5	89.5		0	0	3.0	
07	08	1965	07	03	50	36.5	89.5		C	0	3.3	
12	19	1965	22	19	10	35.9	89.9		0	0	3.6	
02	12	1966	04	32	15	35.9	90.0	25	00	4	3.6	
03	13	1966	14	24	42	36.2	90.0		0	0	3.0	
04	11	1967	23	44	45	36.1	89.7		Ö	Ö	3.0	
07	06	1967	16	43	51	35.8	90.4		ō	0	3.4	
10	18	1967	05	08	36	36.5	89.5		o	0	3.0	
01	23	1968	16	16	00	36.5	89.5		o	0	3.3	
02	10	1968	01	34	32	36.5	89.7		ŏ	3	3.5	
-					-				•	-	4.5	

(Continued)

(Sheet 4 of 5)

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Table 8 (Concluded)

MS	MB	10		AREN	FELT	LON	LAT)	UT	OT		ATE	•
	3.5	0		0		89.5	36.5		59	01	1968		05
	3.0	0		ò		89.5	36.5	25	21	04	1968	15	07
	3.8	4		ō		89.9	35.2	00	45	17	1970	07	01
	3.3	3		ō		89.7	36.5	29	44	03	1970	27	03
	3.0	0		ō		90.0	36.0	35	25	10	1970	05	11
2.9	4.4	6		000	921	90.1	35.9	55	13	02	1970	17	îi
	3.0	4	3-			89.5	36.3	53	46	04	1970	30	11
	3.0	0	•	0		90.0	35.7	00	41	12	1970	14	12
	3.6	4		000	40	89.5	36.7	57	17	10	1970	24	12
	3.0	0		Ö		90.1	35,8	51	00	14	1971	13	04
2.9	4.1	6	5-	000	621	90.4	35.8	39	49	18	1971	01	10
	3.0	0		Ö		89.6	36.7	31	39	06	1971	18	10
	3.7	5		ō		89.6	36.2	32	38	20	1972	29	03
	3.4	4		ō		90.0	35.9	08	12	02	1972	07	05
	3.4	4		ō		90.0	35.0	20	50	03	1973	03	10
	3.7	4		0		89.6	36.5	27	15	20	1973	09	10
	3.4	4		ŏ		89.6	36.2	00	45	10	1973	20	12
	4.3	5		ō		89.4	36.2	37	12	01	1974	08	01
	3.2	0		ō		90.4	35.8	45	53	0.7	1974	24	02
	3.0	0		ō		90.3	35.7	28	24	14	1974	04	03
	3.2	0		Ö		89.8	35.7	29	30	12	1974	12	03
	4.1	6		ŏ		89.4	36.7	19	52	06	1974	13	05
	3.3	5		ŏ		89.6	36.5	58	43	19	1975	13	02
	4.3			Ö		89.7	36.5	27	40	22	1975	13	06
	3.0	Ó		ŏ		89.8	36.0	0 é	11	07	1975	25	08

(Sheet 5 of 5)

Table 9

SOURCE REGION NEW MADRID B

						AKEAS	2/5	DO MM	• • 2				
_	DATE		OT	711)	>	LAT	LON	FELT	ARE	A 1	0	MB	MS
11	09	1820	22	00	00	37.3	89.5		0		5	4.2	0.0
09	05	1839	00	00	00	36.7	88.6		ō		4	3.8	0.0
05	03	1855	03	33	00	37.0	89.2		0		4	3.8	
05	03	1855	10	00	00	37.0	89.2		ō		3	3.4	
07	24	1871	00	00	00	37.0	90.0		0		3	3.4	
02	08	1872	11	00	00	37.0	89.2		0	3-	4	3.6	
07	09	1874	22	00	00	37.0	89.2		0	3-	4	3.6	
01	09	1878	04	30	00	37.0	89.2		0	3-	4	3.6	
07	26	1879	17	45	00	37.0	89.2		0	2-	3	3.4	
07	20	1882	10	00	00	36.9	89.2		0		5	4.2	
01	11	1883	07	12	00	37.0	89.2	2001	000	5-	6	4.6	
04	12	1883	08	30	00	37.0	89.2		0	6-	6	4.0	
07	06	1883	17	15	00	37.0	89.2		0		3	3.4	
07	14	1883	07	30	00	37.0	89.1	250	000	4-	5	4.1	
03	18	1886	05	59	00	37.0	89.2		000		4	4.7	
08	02	1887	18	36	00	37.0	89.2	1700	10 10 100		5	4.7	
09	27	1891	04	55	00	37.0	89.2		0		5	4.2	
10	31	1895	11	08	00	37.0	89.4	25000	000		9	6.2	
11	02	1895	04	16	00	37.0	89.4		0		4	3.8	
11	02	1895	08	00	00	37.0	89.4		0	3-	4	3.6	
11	02	1895	17	00	00	37.0	89.4		0	3-	4	3.6	
11	17	1895	00	00	00	37.0	89.4		0	3-	4	3.6	
05	01	1897	04	00	00	37.0	89.0		0	4-	5	4.0	
20	05	1903	02	56	00	37.0	90.0	1200	000	5-	6	4.6	
10	28	1908	00	27	00	37.0	89.2	130	000	4-	5	4.0	
12	27	1908	21	15	00	37.0	89.0	800	000		4	4.4	
06	09	1913	15	30	00	35.8	88.9	100	000		3	3.9	
02	19	1915	04	35	00	37.1	89.2	9	00		4	3.8	
10	26	1915	07	40	00	36.7	88.6		0		5	4.2	
08	24	1916	09	00	00	37.0	89.2	100	000		4	3.8	
10	19	1916	08	00	00	36.7	88.6		0		3	3.4	
02	17	1918	08	10	00	37.0	89.2	8 (000		3	3.8	
05	07	1920	20	45	00	36,3	88.2	80	000		2	3.8	
02	27	1921	22	16	00	37.0	89.2	80	000		3	3.8	
03	23	1922	21	45	00	37.0	88.9	500	000		4	4.3	
05	06	1923	07	50	00	37.0	89.2		000	3-	4	3.9	
05	15	1923	23	42	00	37.0	99.2	80	000	3-	4	3.8	
11	29	1923	23	20	00	37.0	89.2		0		4	3.8	
03	02	1924	11	18	00	37.0	89.1	800			5	4.4	
05	13	1925	12	00	00	36.7	88.6	100	000	4-	5	3.8	
04	15	1928	15	05	00	37.3	89.5		0		4	3.8	
08	29	1930	06	26	54	37.0	89.1	100			4	4.0	
09	03	1930	12	00	00	37.0	88.9		0		3	3.4	
09	04	1930	05	30	00	37.0	88.9		0		3	3.4	
04	06	1931	15	37	03	36.8	89.0	12	000		4	3.8	
10	24	1933	00	00	00	37.3	89.5	95.	0		3	3.4	
08	20	1934	00	37	27	36.9	89.2	850	0	2-	6	3.2	
08	20	1934	22	41	12	37.3	89.2		0	2-	2	3.0	
12	20	1937	00	49	46	36.1	89.5	650		4-	5	4.4	
02	04	1940	17	33	00	37.2	89.5	090	0		3	3.4	
02	04	7340	1	00	00	0, . 2	04.5				9	3.4	

(Continued)

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Table 9 (Concluded)

MS	MB	0	4	FELT AREA	LON	LAT		UT)	OT		ATE	
	3.8	4		3000	89.1	37.0	00	53	16	1941	21	10
	3.2	3	2-	0	89.5	37.3	00	55	21	1941	22	11
	3.8	4		0	89.2	37.0	00	28	10	1942		08
	4.1	4		28000	89.2	37.0	00	21	80	1945	13	11
	3.2		2-		89.2	37.0	00	23	16		-	01
	3.4		_	Ü	89.2	37.0	00		07		_	05
	3.4			0	89.2	37.0	00		23	1953		05
	4.4			80000	90.3	36.7			_	1954	_	02
	4.2				89.2		40		05	1958		01
	3.2		2-		90.0	36.9				1962	_	
4.1	4.7		-	280000	90.0	36.7	11			1963		03
	3.5			0	90.1	36.7				1963		
	4.4				88.8	37.0	50		00	1963	-	08
	3.0	0		0	89.3	37.1	30			1965		08
	3.2	4		200	89.5	37.3	17		05	1965	-	
	3.8			700	89.2	37.1	54		13	1965	1	00
	3.4			, , ,	89.5	37.4	01		04	1965	11 10 100	08
	3.4			Ö	89.5	37.4	25		06	1965	-	08
	3.2	-		600	89.1	37.0				1972	-	-

regions. In general this area is described by a low density of earthquakes, most of which are of moderate to small magnitude. Table 10 lists the earthquakes in this region.

Focal Depth

- 26. For earthquakes whose focus lies in the earth's crust, there are in general three methods for determining focal depth. One makes use of the travel times of body waves recorded at points very near the epicenter. The second uses the travel-time differences between the direct P wave and a P wave that reflects off the earth's surface in the epicentral region. The third uses the excitation of long period Love and Rayleigh surface waves.
- 27. The density of distribution of seismographs in the central United States has been low. Consequently, it has not been possible to obtain the necessary data for precise focal depth determination using body waves recorded near the epicenter. The best that can be done with the existing data is to determine that the majority of earthquakes lie within the upper 20 km of the crust. Even in regions covered by microearthquake arrays, focal depths can be determined for only larger earthquakes.
- 28. The second method of determining focal depth can only be applied to earthquakes large enough to produce P waves that can be observed on seismographs at distances of 3000 km and greater.

Table 10 FROM COPY FURNISHED TO DDC

SOURCE REGION RESIDUAL EVENTS AREA= 6185019 KM++2

					,	ARCA=	01850	T NW					
-	DATE		OT	UT)	LAT	LON	FELT	ARE		0	мв	MS
04		818	20	00	00	38.6	90.2		0	3-	4	3.6	0.0
05		823	00	00	00	41.5	A1.0		G		4	3.8	0.0
07		827	11	30	00	30.3	85.8	4500	000		4	4.8	
08		827	04	30	00	38.3	85.8		0		6	4.7	0.0
08	-	827	00	00	00	36.6	90.2		0		3	3.4	0.0
03		828	03	00	CO	38.7	93.8	5500	000		5	4.8	0.0
05	00 1	829	00	00	00	35.6	88.8		0		0	3.0	0.0
02		833	00	00	00	42.3	85.6	200	000		6	4.7	0.0
07	08 1	836	00	00	00	41.5	81.7		0		4	3.8	0.0
02	14 1	843	00	00	00	29.9	90.1		0		0	3.0	
08	09 1	843	00	00	00	35.8	88.2	400	000	3 -	4	4.2	
11	28 1	844	13	00	00	36.0	83.9		0		6	4.7	
04	05 1	850	02	05	00	38.3	85.8		0		5	4.2	
10	01 1	850	00	00	00	41.4	82.3		0		4	3.8	
02		854	00	00	00	37.2	83.8		0	3 -	4	3.6	
02		854	00	00	00	37.2	83.8		0	3 -	4	3.6	
02		854	00	00	00	37.6	84.5	200		4 -	5	4.2	
03		854	00	00	00	38.2	85.2		0		4	3.8	
03		857	00	00	00	41.7	81.2		0	4 -	5	4.0	
04		858	12	00	00	41.7	81.3		0		4	3.8	
00		860	0.0	00	00	46.0	94.8		0	6 -	7	5.0	
01		867	00	0.0	00	41.5	81.7		0		3	3.4	
02		869	00	00	00	38.1	84.5		0		5	4.2	
04		869	00	00	00	42.7	80.8		0		3	3.4	
02		872	14	00	00	43.5	A3.8		0		5	4.2	
07		872	0.5	30	00	39.8	93.5		0		4	3.8	
07		872	00	30	00	41.4	82.1		0	3-	4	3.8	
05		873 876	04	00	00	41.9	97.7		Ö	3-	0	3.0	
01		876	00	00	00	42.4	83.2		Ö		0	3.0	
01	100000000000000000000000000000000000000	877	21	00	00	38.8	83.5	26	00		3	3.4	
06		877	00	00	00	37.5	85.7	۷.	0	4	3	3.4	
08		877	16	50	00	42.3	83.3		00	4-	5	4.0	
03		879	00	00	UO	39.6	99.1		0	4-	5	4.0	
11		880	20	00	00	35.6	87.3		0		3	3.4	
12		880	07	15	00	49.0	97.2		O	3-	4	3.6	
04		881	00	0.0	00	41.6	85.8		C		4	3.8	
05		881	15	00	00	38.9	95.2		0		3	3.4	
08		881	05	00	00	39.2	83.7		0		3	3.4	
04		882	05	00	00	29.9	90.1		0		3	3.4	
10		882	22	15	00	33.6	95.6	5000	00		8	5.5	
11		882	03	15	00	38.6	90.2		0		3	3.6	
02	04 1	883	11	00	00	42.3	85.6	4000	00		4	4.7	
05		883	04	30	00	38.4	82.6		0		4	3.8	
11		883	03	14	00	36.7	90.2		0		4	3.8	
01		885	11	30	00	41.3	81.1		0		3	3.4	
02		885	00	00	00	37.2	94.3		U	-	3	3.4	
07		885	00	00	00	35.2	88.2		0	3-	4	3.6	
08		885	05	05	00	41.3	A1.1		0	2-	2	3.2	
12		885	01	05	00	40.4	89.0		0		3	3.4	
01	22 1	886	16	38	00	30.4	92.0		U		U	3.0	

(Continued)

(Sheet 1 of 8)

Table 10 (Continued)

DATE													
05 03 1886 03 00 39.5 92.1 1000 3-4 3.6 08 14 1886 00 00 39.7 98.1 1000 3-4 3.6 06 06 1889 16 25 00 35.9 98.3 0 3-4 3.6 07 27 1895 00 00 35.2 98.3 0 3.3.4 3.6 06 06 1898 08 30 00 37.7 84.3 0 3.3.4 06 26 1898 08 30 00 37.7 84.3 0 3.3.4 06 26 1898 00 00 41.5 81.7 0 3-4 3.6 02 91 1899 00 00 41.9 87.6 0 3.3.4 10 11 1899 14 00 00 34.1 98.5 1700 43.8 11 12 1899 14 00 00 34.5 89.5 <		DATI	E	OT	(UT)		LON	FELT AREA		10	MB	MS
08 14 1886 00 00 00 39.7 86.1 10000 3-4 3.6 06 06 1889 16 25 00 35.9 88.1 10000 3-4 3.9 01 08 1891 06 00 00 31.7 95.2 0 7 3.8 07 27 1895 00 00 00 03 35.2 88.3 0 3-4 3.6 03 30 1898 01 30 03 36.8 85.8 0 3 3.4 06 26 1898 08 30 00 37.7 84.3 0 3 3.4 06 26 1898 08 30 00 37.7 84.3 0 3 3.4 06 26 1898 08 30 00 37.7 84.3 0 3 3.4 00 24 1898 00 00 00 441.5 81.7 0 3-4 3.6 03 14 1900 03 00 00 42.1 96.5 1700 4 3.8 11 12 1899 14 00 00 34.3 83.0 0 4 3.8 03 14 1900 03 00 04 45.5 89.5 0 3-4 3.6 03 14 1900 05 00 00 45.5 89.5 0 3-4 3.6 03 14 1900 05 00 00 45.5 89.5 0 3-4 3.6 03 14 1900 03 00 00 45.5 89.5 0 3-4 3.6 04 09 1900 14 00 00 41.4 81.8 0 64.7 01 04 1901 03 12 00 37.8 89.0 0 5000 5 4.2 05 124 1902 10 10 00 03 39.9 85.2 0 3-4 3.6 04.7 03 10 1902 06 00 00 35.1 85.3 0 5000 5 4.2 05 124 1902 10 13 00 39.9 85.2 0 3-4 3.6 03 12 1902 11 30 03 39.9 85.2 0 3-4 3.6 03 12 1902 11 30 03 39.9 85.2 0 3-4 3.6 00 10 11 1903 28 45 00 39.9 85.2 0 3-4 3.6 00 10 11 1903 28 45 00 39.9 85.2 0 3-4 3.6 00 10 11 1903 28 45 00 39.9 85.2 0 3-4 3.6 00 10 11 1903 28 45 00 39.9 85.2 0 3-4 3.6 00 10 11 1903 18 30 00 39.9 85.2 0 3-4 3.6 00 10 11 1903 18 30 00 39.9 85.2 0 3-4 3.6 00 10 11 1903 18 30 00 39.9 85.2 0 3-4 3.6 00 10 11 1903 18 50 00 39.9 85.2 0 3-4 3.6 00 10 11 1903 18 50 00 39.9 85.2 0 3-4 3.6 00 31.1 85.3 0 5 4.2 00 10 11 1903 18 50 00 39.9 85.2 0 2-3 3.2 00 10 11 1903 16 30 00 40.3 81.4 86.3 0 5 4.2 00 10 11 1903 16 30 00 40.4 91.6 13 100.2 5 4.2 00 10 11 1903 16 30 00 40.4 91.6 13 100.2 5 4.2 00 10 11 1903 16 30 00 44.1 87.7 0 5 4.2 00 10 11 1903 16 30 00 44.1 87.7 0 5 4.2 00 10 11 1903 16 30 00 44.1 87.7 0 0 3.0 0 39.4 86.3 0 0 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00 39.9 85.2 0 2-3 3.2 0 0 3.4 3.6 00	03	01	1886	16	00	00					4	3.6	
06 1889 16 25 U0 35 99	05	03	1886	03	00	00		92.1	1000	3 -	4	3.6	
01 08 1891 06 00 00 31.7 99.2 0 7 3.8 07 27 1895 00 00 00 03 36.8 85.8 0 3 .4 3.6 08 1898 01 30 00 37.7 84.3 0 3 3.4 06 06 1898 08 30 00 37.7 84.3 0 3 3.4 06 26 1898 08 30 00 37.7 84.3 0 3 3.4 10 24 1898 00 00 00 41.5 81.7 0 3-4 3.6 07 20 19 1899 04 00 00 42.1 86.5 1700 4 3.8 11 12 1899 14 00 00 39.3 83.0 0 4 3.8 11 12 1899 14 00 00 39.3 83.0 0 4 3.8 03 14 1900 03 00 04 45.5 89.5 0 3-4 3.6 03 14 1900 03 00 04 45.5 89.5 0 3-4 3.6 03 14 1900 03 00 04 45.5 89.5 0 3-4 3.6 03 14 1900 03 00 00 45.5 89.5 0 3-4 3.6 03 17 1901 07 00 00 39.3 82.5 25000 5 4.2 01 24 1902 10 48 00 38.6 90.2 130000 6 4.7 01 04 1901 03 12 00 37.8 94.0 5000 5 4.2 01 24 1902 10 48 00 38.6 90.2 130000 6 4.7 01 04 1901 03 12 00 37.8 94.0 5000 5 4.2 01 24 1902 11 30 00 39.9 85.2 0 3-4 3.6 03 12 1902 17 30 00 35.1 85.3 0 5 4.2 01 18 1902 22 00 00 35.1 85.3 0 5 4.2 01 1903 18 30 03 9.9 85.2 0 3-4 3.6 03 17 1903 18 30 03 9.9 85.2 0 3-4 3.6 03 17 1903 18 30 03 9.9 85.2 0 3-4 3.6 03 12 1902 17 30 00 39.4 86.3 0 5 4.2 01 1903 18 30 03 9.9 98.2 0 2-3 3.2 01 13 1903 14 53 00 39.9 85.2 0 2-3 3.2 01 11 1903 18 30 03 39.9 85.2 0 2-3 3.2 01 11 1903 18 30 03 39.9 85.2 0 2-3 3.2 01 11 1903 18 30 00 39.4 86.3 0 3 03 17 1903 00 00 00 37.1 89.5 0 3-4 3.6 07 27 1905 16 30 00 40.4 8.6 9.0 07 27 1905 16 30 00 40.4 8.6 9.0 07 27 1905 16 30 00 47.3 88.4 4000 7 7 5.0 08 22 1905 10 45 00 39.7 92.3 0 0 3 3.4 08 22 1905 10 45 00 39.7 92.3 0 0 3 3.4 09 1906 05 15 00 39.7 92.3 0 0 3.0 09 1906 06 38 00 39.5 85.7 0 0 3.0 05 19 1906 09 20 00 42.9 85.7 0 0 3.0 05 19 1906 09 20 00 42.9 85.7 0 0 3.0 05 19 1906 09 20 00 42.9 85.7 0 0 3.0 05 19 1906 09 20 00 47.3 88.4 30000 0 3.8 06 1906 1906 1900 00 39.7 98.8 07 19 1906 09 20 00 42.9 85.7 0 0 3.0 07 27 1906 19 10 00 00 38.7 88.4 08 1906 00 00 00 00 47.3 88.4 09 1906 00 00 00 00 47.3 88.4 00 3 3.4 00 3 3.4 00 3 3.4 00 3 3.4 00 3 3.4 00 3 3.4 00 3 3.4 00 3 3.4 00 3 3.4 00 3 3.4 00 3 3.4 00 3 3.4 00 3 3.4 00 3 3.4	08	14	1886	00	00	00	39.7	96.1	0	3-		3.6	
07 27 1895 00 00 00 35.2	06	06	1889	16	25			A8.1	10000	3-		3.9	
03	01	08	1891	06	00	00	31.7	95.2					
96 06 1898 08 30 00 37.7 84.3 0 3 3.4 10 24 1898 08 30 00 37.7 84.3 0 3-4 3.6 12 24 1898 00 00 00 41.5 81.7 0 3-4 3.6 12 1899 04 00 00 42.1 96.5 1700 4 3.8 12 11 12 1899 14 00 00 39.3 83.0 0 4 3.8 12 01 1899 14 00 03 45.5 89.5 0 3-4 3.6 03 14 1900 05 00 045.5 89.5 0 3-4 3.6 03 14 1900 00 45.5 89.5 0 3-4 3.6 03 14 1900 00 45.5 89.5 0 3-4 3.6 05 17 1901 07 00 <td< td=""><td>07</td><td>27</td><td>1895</td><td>00</td><td>00</td><td>00</td><td>35.2</td><td>98.3</td><td>0</td><td>3 -</td><td></td><td>3.6</td><td></td></td<>	07	27	1895	00	00	00	35.2	98.3	0	3 -		3.6	
06 26 1898 08 30 00 37.7 84.3	03	30	1898	01	30	00		85.8	0		3		
10 24 1898 00 00 00 41.5	96	06	1898	08	30	00		84.3	0			3.4	
02 09 1899 00 00 00 41.9 87.6 0 0 3.0 11 1899 04 00 00 42.1 96.5 1700 4 3.8 11 12 1899 14 00 00 39.3 83.0 0 4 3.8 12 01 1899 18 50 00 36.8 94.4 0 3.8 03 14 1900 05 00 00 45.5 89.5 0 3-4 3.6 03 14 1900 05 00 00 45.5 89.5 0 3-4 3.6 04 09 1900 14 00 00 41.4 81.8 0 6 4.7 01 04 1901 03 12 00 37.8 94.0 5000 5 4.2 05 17 1901 07 00 00 39.3 82.5 25000 5 4.2 01 24 1902 10 48 00 38.6 90.2 130000 6 4.7 03 10 1902 06 00 00 45.5 89.5 0 3-4 3.6 03 12 1902 11 30 00 39.9 85.2 0 3-4 3.6 05 29 1902 07 30 00 35.1 85.3 0 5 4.2 01 24 1902 07 00 00 40.3 81.4 0 4-5 4.0 10 18 1902 22 00 00 35.0 85.3 0 5 4.2 01 01 1903 18 30 00 39.9 85.2 0 3-4 3.6 05 29 1902 27 30 00 35.0 85.3 0 5 4.2 01 01 1903 18 30 00 39.9 85.2 0 2-3 3.2 01 01 1903 18 50 00 39.9 85.2 0 2-3 3.2 01 01 1903 18 50 00 39.9 85.2 0 2-3 3.2 01 13 1903 14 53 00 38.8 95.3 0 5 4.2 01 1903 11 50 00 39.4 86.3 0 4-5 4.0 10 18 1903 23 45 00 39.9 85.2 0 2-3 3.2 01 13 1903 10 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.7 91.4 0 2-3 3.2 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0	06	26	1898	08	30	00	37.7	84.3	. 0		3	3.4	
02 09 1899 00 00 00 41.9 87.6 0 0 3.0 11 1899 04 00 00 42.1 96.5 1700 4 3.8 11 12 1899 14 00 00 39.3 83.0 0 4 3.8 12 01 1899 18 50 00 36.8 94.4 0 3.8 03 14 1900 05 00 00 45.5 89.5 0 3-4 3.6 03 14 1900 05 00 00 45.5 89.5 0 3-4 3.6 04 09 1900 14 00 00 41.4 81.8 0 6 4.7 01 04 1901 03 12 00 37.8 94.0 5000 5 4.2 05 17 1901 07 00 00 39.3 82.5 25000 5 4.2 01 24 1902 10 48 00 38.6 90.2 130000 6 4.7 03 10 1902 06 00 00 45.5 89.5 0 3-4 3.6 03 12 1902 11 30 00 39.9 85.2 0 3-4 3.6 05 29 1902 07 30 00 35.1 85.3 0 5 4.2 01 24 1902 07 00 00 40.3 81.4 0 4-5 4.0 10 18 1902 22 00 00 35.0 85.3 0 5 4.2 01 01 1903 18 30 00 39.9 85.2 0 3-4 3.6 05 29 1902 27 30 00 35.0 85.3 0 5 4.2 01 01 1903 18 30 00 39.9 85.2 0 2-3 3.2 01 01 1903 18 50 00 39.9 85.2 0 2-3 3.2 01 01 1903 18 50 00 39.9 85.2 0 2-3 3.2 01 13 1903 14 53 00 38.8 95.3 0 5 4.2 01 1903 11 50 00 39.4 86.3 0 4-5 4.0 10 18 1903 23 45 00 39.9 85.2 0 2-3 3.2 01 13 1903 10 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.7 91.4 0 2-3 3.2 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.4 3.6 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0 3 3.0 0	10	24	1898	00	00	00	41.5	81.7	0	3 -	4	3.6	
10 11 1899 04 00 00 42.1 96.5 1700 4 3.8 11 12 1899 14 00 00 39.3 83.0 0 4 3.8 12 01 1899 18 50 00 36.8 94.4 0 4 3.8 03 14 1900 05 00 00 45.5 89.5 0 3- 4 3.6 04 09 1900 14 00 00 41.4 81.8 0 6 4.7 01 04 1901 03 12 00 37.8 94.0 5000 5 4.2 05 17 1901 07 00 00 37.8 94.0 5000 5 4.2 05 17 1901 07 00 00 39.3 82.5 25000 5 4.2 01 24 1902 10 48 00 38.6 90.2 130000 6 4.7 03 10 1902 06 00 00 39.3 82.5 25000 5 4.2 05 12 1902 11 30 00 39.9 85.2 0 3- 4 3.6 05 29 1902 07 30 00 35.1 85.3 0 5 4.2 05 14 1902 20 00 03 35.1 85.3 0 5 4.2 05 16 1902 11 30 00 39.9 85.2 0 3- 4 3.6 05 12 1902 13 30 00 35.1 85.3 0 5 4.2 05 10 1903 18 30 00 39.9 85.2 0 2- 3 3.2 05 10 1903 18 30 00 39.9 85.2 0 2- 3 3.2 05 10 1903 18 30 00 39.9 85.2 0 2- 3 3.2 05 10 1903 18 30 00 39.9 85.2 0 2- 3 3.2 05 10 1903 14 53 00 38.8 95.3 0 5 4.2 05 17 1903 17 50 00 39.1 89.5 0 2 2 3.0 03 17 1903 11 50 00 39.1 88.5 0 2 3.0 03 17 1903 11 50 00 39.1 88.5 0 2 3.0 03 17 1903 11 50 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 03 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.7 88.4 00 00 00 00 39.7 90.4 0 2- 3 3.2 0 00 00 00 00 00 00 00 00 00 00 00 00	02	09	1899	00	00	00	41.9	87.6	0		0	3.0	
12 01 1899 18 50 00 36.8 94.4 0 4 3.8 03 14 1900 05 00 00 45.5 89.5 0 3- 4 3.6 04 09 1900 14 00 00 41.4 81.8 0 6 4.7 01 04 1901 03 12 00 37.8 94.0 5000 5 4.2 01 24 1902 10 48 00 38.6 90.2 130000 6 4.7 03 10 1902 06 00 00 39.3 82.5 25000 5 4.2 03 10 1902 06 00 00 39.9 85.2 0 3- 4 3.6 05 29 1902 07 30 00 35.1 85.3 0 5 4.2 01 01 1902 07 00 00 35.1 85.3 0 5 4.2 01 01 1902 07 00 00 35.1 85.3 0 5 4.2 01 01 1903 18 30 00 39.9 85.2 0 3- 4 3.6 05 29 1902 27 00 00 35.0 85.3 0 5 4.2 01 13 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 13 1903 14 53 00 38.8 95.3 0 5 4.2 01 13 1903 14 53 00 38.8 95.3 0 5 4.2 01 13 1903 10 00 00 39.4 86.3 0 4 3.6 09 20 1903 00 00 00 39.4 86.3 0 3 3.4 3.6 09 20 1903 00 00 00 39.4 86.3 0 4 3.8 0 3 3.4 12 11 1903 00 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 00 37.5 100.2 7000 5 4.2 03 13 1905 16 30 00 40.4 91.6 13000 4- 5 4.0 02 24 1906 05 15 00 39.7 92.3 0 3 3.4 3.8 04 22 1905 10 45 00 39.9 91.4 0 2- 3 3.2 0 0 3 3.4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10	11	1899	04	00	00	42.1		1700		4	3.8	
12 01 1899 18 50 00 36.8 94.4 0 4 3.8 03 14 1900 05 00 00 45.5 89.5 0 3- 4 3.6 04 09 1900 14 00 00 41.4 81.8 0 6 4.7 01 04 1901 03 12 00 37.8 94.0 5000 5 4.2 01 24 1902 10 48 00 38.6 90.2 130000 6 4.7 03 10 1902 06 00 00 39.3 82.5 25000 5 4.2 03 10 1902 06 00 00 39.9 85.2 0 3- 4 3.6 05 29 1902 07 30 00 35.1 85.3 0 5 4.2 01 01 1902 07 00 00 35.1 85.3 0 5 4.2 01 01 1902 07 00 00 35.1 85.3 0 5 4.2 01 01 1903 18 30 00 39.9 85.2 0 3- 4 3.6 05 29 1902 27 00 00 35.0 85.3 0 5 4.2 01 13 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 13 1903 14 53 00 38.8 95.3 0 5 4.2 01 13 1903 14 53 00 38.8 95.3 0 5 4.2 01 13 1903 10 00 00 39.4 86.3 0 4 3.6 09 20 1903 00 00 00 39.4 86.3 0 3 3.4 3.6 09 20 1903 00 00 00 39.4 86.3 0 4 3.8 0 3 3.4 12 11 1903 00 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 00 37.5 100.2 7000 5 4.2 03 13 1905 16 30 00 40.4 91.6 13000 4- 5 4.0 02 24 1906 05 15 00 39.7 92.3 0 3 3.4 3.8 04 22 1905 10 45 00 39.9 91.4 0 2- 3 3.2 0 0 3 3.4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	11	12	1899	14	00	00	39.3	83.0	0		4	3.8	
03 14 1900 05 00 00 45.5 49.5 0 3- 4 3.6 04 09 1900 14 00 00 41.4 81.8 0 6 4.7 01 04 1901 03 12 00 37.8 94.0 5000 5 4.2 05 17 1901 07 00 00 39.3 82.5 25000 5 4.2 01 24 1902 10 48 00 38.6 90.2 130000 6 4.7 03 10 1902 06 00 00 39.9 85.2 0 3- 4 3.6 05 29 1902 11 30 00 39.9 85.2 0 3- 4 3.6 05 29 1902 07 30 00 35.1 85.3 0 5 4.2 06 14 1902 07 00 00 40.3 81.4 0 4- 5 4.0 10 18 1902 22 00 00 35.0 85.3 0 5 4.2 01 01 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 01 1903 23 45 00 39.9 85.2 0 2- 3 3.2 01 13 1903 14 53 00 39.9 85.2 0 2- 3 3.2 01 13 1903 14 53 00 39.9 85.2 0 2- 3 3.2 01 13 1903 15 50 00 39.1 89.5 0 2 2- 3 3.2 01 13 1903 00 00 00 39.1 89.5 0 3- 4 3.6 09 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 88.5 0 2 3.0 10 28 1904 00 00 00 39.4 88.5 0 2 3.0 10 28 1904 00 00 00 39.4 88.5 0 2 3.0 10 28 1904 00 00 00 39.4 88.5 0 2 3.0 10 28 1906 00 00 00 39.4 88.5 0 2 3.0 10 28 1906 00 00 00 39.4 88.5 0 2 3.0 10 28 1906 00 00 00 39.4 88.5 0 2 3.0 10 28 1906 00 00 00 39.4 88.5 0 2 3.0 10 28 1906 00 00 00 39.4 88.3 0 4 3.8 10 20 1905 16 30 00 40.4 91.6 13000 4- 5 4.0 10 20 1905 16 30 00 40.4 91.6 13000 4- 5 4.0 10 20 1906 00 39.7 92.3 0 3 3.4 10 20 1906 18 30 00 41.5 81.7 0 4 3.8 10 20 1906 00 80 00 90 39.7 91.4 0 4 3.8 10 20 1906 18 30 00 41.5 81.7 0 0 3.0 10 20 1906 00 10 00 44.4 81.6 1000 5 4.2 10 1906 00 10 00 44.4 81.6 1000 5 4.2 10 10 1906 00 10 00 47.3 88.4 0 5 4.3 10 1906 00 10 00 44.4 81.6 1000 5 4.2 10 1906 00 10 00 47.3 88.4 0 5 4.3 10 1906 00 10 00 47.3 88.4 0 5 4.3 10 1906 00 10 00 44.4 81.6 1000 5 4.2 10 1906 00 10 00 47.1 88.4 0 0 0 3.0 10 1906 00 10 00 47.1 88.4 0 0 0 3.0 10 24 1906 05 15 00 39.7 92.3 0 0 3.3 3.4 10 19 1906 00 5 15 00 39.7 92.3 0 0 3.0 3 3.4 3 3.4 3 3.4 3 3.4 3 3.4 3 3.4 3 3.4 3 3.4 3 3.5 3 3.5 3 3.5 4 3.6 4 3.6 4 3.8 4 3.6 5 4.2 5 5 4.2 5 5 6 6 6 6 6 7 6 7 6 7 6 7 6 7 6 7 6 7	12	01	1899	18	50	00	36.8	94.4	0		4	3.8	
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01 04 1901 03 12 00 37.8 94.0 5000 5 4.2 05 17 1901 07 00 00 39.3 82.5 25000 6 4.7 03 10 1902 06 00 00 39.9 85.2 0 3- 4 3.6 05 29 1902 07 30 00 35.1 85.3 0 5 4.2 06 14 1902 27 00 00 40.3 81.4 0 4- 5 4.0 10 18 1902 27 00 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 50 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 50 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 50 00 39.9 85.2 0 2- 3 3.2 01 01 1903 16 50 00 39.1 89.5 0 3- 4 3.6 09 20 1903 00 00 00 39.4 86.3 0 3.4 3.8 11 20 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.4 86.3 0 3 3.4 12 11 1903 00 00 00 39.1 88.5 0 2 3.0 10 28 1904 00 00 00 39.1 88.5 0 2 3.0 10 28 1905 16 30 00 40.4 91.6 13000 4- 5 4.2 08 22 1905 10 45 00 39.9 91.4 0 2- 3 3.2 08 22 1905 10 45 00 39.9 91.4 0 2- 3 3.2 09 20 1906 05 15 00 39.7 92.3 0 3.0 05 08 1906 06 58 00 39.5 85.8 6000 3- 4 3.6 05 09 1906 06 38 00 39.2 85.9 0 4 3.8 05 19 1906 09 20 00 42.9 85.7 0 0 3.0 05 08 1906 06 58 00 39.5 85.8 6000 3- 4 3.6 05 09 1906 09 10 00 00 38.7 88.4 0 5 4.2 08 08 1906 01 10 00 00 38.7 88.4 0 5 4.3 08 13 1906 12 10 00 40.4 81.6 1000 5 4.2 08 08 1906 03 1900 00 47.3 88.4 30000 0 3.0 08 10 10 10 10 10 10 10 10 40.4 81.6 1000 5 4.2 08 08 1906 03 1900 00 47.3 88.4 30000 0 3.0 08 10 10 10 10 10 10 10 10 10	03	14	1900	05	00	00	45.5	49.5	0	3 -	4	3.6	
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03 10 1902 06 00 00 39.9 85.2 0 3- 4 3.6 05 29 1902 07 30 00 35.1 85.3 0 5 4.2 06 14 1902 07 00 00 40.3 81.4 0 4- 5 4.0 10 18 1902 22 00 00 35.0 85.3 0 5 4.2 01 01 1903 18 30 00 39.9 85.2 0 2- 3 3.2 01 01 1903 18 50 03 39.9 85.2 0 2- 3 3.2 01 01 1903 11 50 00 38.8 95.3 0 2 3.0 03 17 1903 11 50 00 39.1 89.5 0 3- 4 3.6 09 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.4 86.3 0 4 3.8 11 20 1903 00 00 00 39.1 88.5 0 2 3.0 10 28 1904 00 00 00 37.5 100.2 7000 5 4.2 03 13 1905 16 30 00 40.4 91.6 13000 4- 5 4.0 07 27 1905 00 20 00 47.3 88.4 40000 7 5.0 08 22 1905 10 45 00 39.9 91.4 0 2- 3 3.2 02 24 1906 05 15 00 39.7 92.3 0 3.0 05 08 1906 06 58 00 39.7 91.4 0 2- 3 3.2 05 09 1906 06 58 00 39.9 85.8 0 0 3.0 05 08 1906 06 58 00 39.7 91.4 0 2- 3 3.2 05 09 1906 06 58 00 39.5 85.8 6000 3- 4 3.8 05 19 1906 06 92 00 42.9 85.7 0 3.0 06 1906 09 20 00 47.3 88.4 0 5 4.3 06 27 1906 12 10 00 40.4 81.6 1000 5 4.2 08 08 1906 00 00 00 38.7 88.4 0 5 4.3 06 27 1906 12 10 00 40.4 81.6 1000 5 4.2 08 08 1906 00 10 00 38.7 88.4 0 5 4.3 08 13 1906 13 19 00 39.7 88.8 0 0 4 3.8 08 13 1906 13 19 00 39.7 88.8 0 0 4 3.8 08 13 1906 13 19 00 39.7 88.8 0 0 4 3.8 08 13 1906 13 19 00 39.7 88.8 0 0 0 33.0 08 19 1906 00 10 00 47.3 88.4 0 5 4.3 08 13 1906 13 19 00 39.7 88.8 0 0 0 33.0 08 19 1906 00 10 00 47.3 88.4 0 5 4.3 08 13 1906 13 19 00 39.7 88.8 0 0 0 33.0	05	17	1901	07	00	00	39.3	82.5	25000		5	4.2	
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	04	12	1907	00	00	00	41.5	81.7	0		3	3.0	

(Continued)

(Sheet 2 of 8)

THIS PACE IS BEST QUALITY PRACTICABLE FROM COPY FURNISHED TO DDC

Table 10 (Continued)

	DATE		1000	(UT		LAT	LON	FELT ARE		МВ	MS
12	11	1907	04	32	00	38.6	90.2	0	4	3.8	
11	12	1908	00	00	00	38.7	93.2	1800	4	3.8	
01	23	1909	03	15	00	47.2	88.6	0	5	3.4	
07	19	1909	04	34	00	40.2	90.0	100000	7	5.3	
09	22	1909	00	00	00	36.7	86.5	10000	5	4.2	
10	22	1909	00	00	00	38.9	84.5	0	U	3.0	
05	08	1910	17	30	00	30.1	96.0	0	4	3.8	
05	12	1910	00	00	00	30.1	96.0	2500	4	3.8	
02	28	1911	09	00	00	38.7	90.3	0	4	3.8	
07	29	1911	00	00	00	41.8	87.6	0	4- 5	3.2	
03	28	1913	21	50	00	36.2	83.7	7000	7	5.3	
11	11	1913	14	00	00	38,2	85.8	0	4	3.8	
01	24	1914	03	24	00	35.6	84.5	0	5	4.2	
10	07	1914	21	00	00	43.1	89.4	Ö	4	3.8	
12	30	1914	01	00	00	30.5	95.9	Č	4- 5	3.5	
03	03	1915	07	45	00	47.3	AB.4	ŏ	3- 4	3.6	
08	08	1915	15	15	00	46.1	103.6	o	4	3.8	
	04	1915	14	25	00	47.3			4- 5	4.0	
10						43.1	88.4	0			
05	31	1916	22	45	00		89.3	0	2	3.0	
01	25	1917	22	15	00	35.9	86.8	0	2- 3	3.2	
01	26	1917	13	1.5	00	35.9	86.8	0	2- 3	3.2	
01	27	1917	21	00	00	35.9	86.8	0	2- 3	3.2	
)2	06	1917	17	26	00	47.9	95.0	0	4	3.8	
9	03	1917	21	30	00	46.3	94.8	48000	6	4.7	
01	16	1918	15	45	00	35.9	83.9	0	5	4.2	
02	22	1918	00	00	00	42.8	84.2	0	4	3.8	
36	22	1918	01	00	00	36.1	84.1	8000	5	4.2	
07	01	1918	19	0.2	00	39.7	91.4	0	4	3.8	
10	01	1918	07	38	00	47.3	88.4	0	3	3.4	
10	16	1918	02	15	00	35.2	89.2	100000	5	4.5	
02	29	1920	03	15	00	37.2	93.3	80000	4	4.3	
10	03	1920	14	15	00	38.6	94.3	8000	3	3.8	
12	24	1920	07	30	00	36.0	85.0	0	5	4.2	
09	02	1921	14	00	00	30.2	86.3	Ö	3	3.4	
9	21	1921	00	0.0	00	36.0	86.1	Ğ	3	3.4	
12	15	1921	13	20	00	35.8	84.6	ő	5	4.2	
3	16	1922	09	30	00	43.0	82.5	ő	3	3.4	
		1922	04	20				0	4	7.0	
3	30			1100 100	00	35.5	86.7		2	3.8	
14	11	1922	05	00	00	40.9	90.6	0		3.0	
7	07	1922	00	00	00	43.8	98.5	0	. 5	4.2	
3	07	1923	05	03	00	31.7	106.5	50000	4- 5	4.3	
3	27	1923	08	00	00	34.6	89.7	10000	3- 4	3.9	
11	10	1923	04	00	00	40.0	89.9	1600	5	4.2	
11	28	1923	12	30	00	37.5	87.3	0	3	3.4	
9	24	1924	11	00	00	40.9	100.1	0	4	3.8	
01	26	1925	80	34	00	42.5	72.4	500	2	3.2	
1	27	1925	22	42	00	36.2	91.7	6000	3	3.8	
03	03	1925	16	20	00	42.1	87.7	0	2- 3	3.2	
14	04	1925	00	00	00	39.1	84.5	0	0	3.0	
7	08	1925	16	00	00	30.2	93.2	10000	4	3.8	
7	13	1925	00	00	00	38.8	90.0	0	5	4.2	

(Continued) (Sheet 3 of 8)

	DAT	E	OT	(UT)	LAT	LON	FELT	AREA		10	MB	MS
07	29	1925	11	30	00	34.5	101.2	-	0		4	3.8	
07	30	1925	08	00	00	34.5	100.3		0		5	4.2	
03	10	1926	00	00	00	36.8	101.7		0		0	3.0	
10	28	1926	08	42	00	41.7	83.6		ō		3	3.4	
10	28	1926	11	00	60	41.7	A3.6		ō		4	3.8	
11	05	1926	15	53	00	39.1	92.1		00	4-	7	4.0	
01		1927	12	00	00	34.7				0-	5	4.2	
	16	1927		30	00	46 7	86.0	0:	500		4	3.8	
01	17		05			40.7	92.5		0				
02	17	1927	06	00	00	40.7	82.5		0		2	3.0	
03	18	1927	17	25	00	39.9	95.3		800		5	4.2	
06	16	1927	12	00	00	34.7	86.0		500		5	4.2	
07	20	1927	00	00	00	35.8	86.0	1800			6	4.7	
10	08	1927	12	56	00	35.0	85.3		0		5	4.2	
10	29	1927	00	0 0	00	40.9	81.2		0		5	4.2	
11	13	1927	16	21	00	32.3	90.2	80	000		4	4.2	
12	15	1927	04	30	00	28.9	A9.4	100	000		4	4.2	
03	07	1928	02	45	00	35.6	87.0	50	000	2-	3	3.4	
03	17	1928	21	15	00	38.6	90.2		200		2	3.3	
09	09	1928	21	00	00	41.5	82.0		000		5	4.2	
11	08	1928	14	15	00	39.5	89.1		0		4	3.8	
12	23	1928	06	10	00	47.6	93.9		ō		4	3.8	
06	10	1929	00	00	00	41.5	91.7		0		3	3.4	
07	28	1929	17	00	00	28.9	89.4	0.0	000		4	3.8	
	1000	1929	19	19	00	41.5		0.			3	3.0	
09	17	1929	04	20	00	37.2	81.5		0		4		
11	27	1930	03	45	00	46.5	99.8		0			3.8	
01	24						84.4		0		3	3.4	
05	28	1930	17	30	00	39.7	91.4		0		3	3.4	
08	08	1930	18	31	00	39.7	91.4		Ü		4	3.8	
08	30	1930	09	28	00	35.9	84.4		0		0	3.0	
10	16	1930	00	00	00	36.0	83.9		0		5	4.2	
10	19	1930	12	12	00	30.1	91.0	500			6	4.7	
11	20	1930	00	0 0	00	42.6	83.4		0		3	3.4	
12	23	1930	14	44	00	38.5	90.7		00		4	3.8	
08	09	1931	06	18	37	39.1	94.7	E	00	4-	5	4.0	
08	09	1931	07	07	00	39.1	94.7		0		0	3.0	
08	09	1931	07	15	00	39.1	94.7		0		U	3.0	
08	16	1931	11	40	21	30.6	104.1	14000	00		8	5.6	
08	16	1931	19	33	00	30.6	174.1		0		0	3.0	
08	19	1931	02	36	00	30.6	104.1		0		6	0.	
08	19	1931	02	36	00	30.6	104.1		Ü		5	4.2	
08	26	1931	00	00	00	30.6	104.1		0		3	3.4	
10	02	1931	00	00	00	31.7	106.5			2-	3	3.2	
10	18	1931	21	12	00	43.1	89.4		0	-	3	3.4	
11	03	1931	15	50	00	29.9	104.2		Ö		2	3.2	
11	27	1931	09	23	00	36.2	86.8		Ü		3	3.4	
	17	1931	03	36	00			2000	-		7	5.4	
12	17	1931	21	08	19		89.9	2200		6-	2	5.0	
12			-				90.2		0				
01	22	1932	00	00	00	41.1	81.5		0		5	4.2	
01	29	1932	00	15	00	39.0	99.6		00		5	4.2	
04	09	1932	10	15	00	31.5	96.0	55		5-	6	4.0	
01	29	1932	11	00	00	46.4	85.5		0		2	3.0	

(Continued)

(Sheet 4 of 8)

THIS PAGE IS BEST QUALITY PRACTICABLE FROM COPY FURNISHED TO DDC Table 10 (Continued)

-	DATE	:	OT	(UT	,	LAT	LON	FELT AREA	1	0	MB	MS
02	20	1933	17	00	00	39.8	99.9	15000		5	4.2	
05	28	1933	15	10	00	38.6	83.7	1600		5	4.2	
11	16	1933	09	29	01	38.6	90.6	4000		4	3.8	
01	30	1935	22	00	00	40.5	94.0	0		3	3.4	
			14	15	00	40.8	91.1	Ö		3	3.4	
02	26	1935		00						4	3.8	
05	26	1935	00		00	41.3		· ·			3.8	
10	00	1935	17	15	00	40.5	87.6	0		3	3.2	
10	29	1935	00	00	00	39.6	90.8	0		0	3.0	
08	08	1936	01	40	00	31.7	106.5	0		3	3.4	
10	08	1936	16	30	00	39.3	84,4	1800		3	3.4	
10	15	1936	17	50	00	31.7	106.5	U			3.8	
12	26	1936	01	15	00	39.1	84.5	U		3 3	3.4	
12	26	1936	0.5	05	00	39.1	84.5	0		3	3.4	
03	30	1937	22	45	00	31.7	106.4	0		3	3.4	
06	29	1937	21	45	00	40.7	89.6	0		3	3.0	
08	05	1937	23	12	00	38.7	90.1	0		3	3.4	
08	08	1937	01	40	00	31.7	106.5	0		3	3.4	
10	17	1937	04	25	00	39.1	84.5	0		3	3.4	
02	12	1938	06	27	00	41.6	87.0	17000		5	4.2	
03	13	1938	16	10	00	42.4	83.2	0		4	3.8	
01	28	1939	17	55	00	46.8	95.8	20000		4	3.8	
06	24	1938	09	00	00	34.7	86.6	0		0	3.0	
06	24	1939	10	27	00	34.7	86.6	1300		4	3.8	
06	24	1939	11	45	00	34.7	86.6	0		0	3.0	
07	18	1939	00	00	00	45.7	87.1	O		U	3.0	
CB	01	1939	00	00	00	45.7	87.1	Ü		0	3.0	
11	07	1939	10	00	00	45.7	87.1	0		3	3.2	
01	08	1940	20	05	00	38.3	85.8	Ö		3	3.4	
05	27	1940	08	30	00	38.2	85.8	Ö		3	3.2	
05	31	1940	17	0.0	00	41,1	91.5	Ö			3.0	
06	16	1940	04	30	00	40.9	A2.3	Ö		2	3.8	
07	28	1940	09	30	00	40.9	82.3	ő		3	3.4	
08	15	1940	10	35	00	40.9	82.3	ŭ		3	3.4	
100000		1940	03	30	00	40.9		Ö		3	3.4	
08	20		100			70.9	82.3					
12	02	1940	16	16	00	33.0	94.0	0		4	3.8	
03	04	1941	00	00	00	36.0	93.9	0	2-	3	3.2	
06	28	1941	18	30	00	32.3	90.8	0		4	3.6	
09	08	1941	09	45	00	35.0	85.3	250		4	3.8	
01	14	1942	18	05	00	38.4	90.3	1500		3	3.4	
01	23	1942	16	00	00	38.6	90.4	0		2	3.0	
01	29	1942	55	12	00	38.3	90.4	U		0	3.0	
01	30	1942	15	00	00	38.7	90.3	0		0	3.0	
09	10	1942	09	0.0	00	36.8	99.3	0		4	3.8	
11	17	1942	18	18	00	36.6	90.2	500		4	3.8	
11	18	1942	00	10	00	36.6	94.2	0		0	3.0	
12	27	1942	20	40	00	38.6	90.3	0		3	3.2	
02	09	1943	23	21	00	45.2	88.2	0		3	3.2	
02	15	1943	12	00	00	45.7	87.1	0		0	3.0	
03	09	1943	03	25	24	42.2	80.9	220000		5	4.7	
04	13	1943	17	00	00	36.3	85.8	0		4	3.8	
04	18	1943	80	36	00	38.3	85.8	0		4	3.8	

(Continued)

(Sheet 5 of 8)

Table 10 (Continued)

05	-	DAT	E	OT	(UT	,	LAT	LON	FELT	AREA	10	MB	MS
05						00	36.9				2	3.0	
0.0 0.8 1943 19 50 0.0 36.6 90.4	05	24	1943	20	33	00	38.9	90.2		0	2	3.0	
07 25 1943 06 49 10 36.1 91.3	06	08	1943	19	50	00	36.6			U	3- 4	3.6	
11 16 1944 19 35 00 45,7 87.1 0 2- 3 3.2 12 10 1944 11 00 00 45,7 87.1 0 4 3.8 0.8 1945 01 45 58 38.6 90.2 8000 3 3.4 05 18 1945 07 51 00 36.6 90.2 0 4 3.8 0.8 01 1945 07 51 00 36.6 90.2 0 4 3.8 0.8 01 026 1946 20 37 00 48.1 103.6 0 4 3.8 0.9 0.7 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	07	25	1943	06	49	10	35.1	91.3		U	4- 5	4.0	
12 10 1944 11 00 00 45.7 87.1 0 4 3.8 03 28 1945 01 45 58 38.6 90.2 8000 3 3.4 05 18 1945 14 26 00 45.7 87.1 0 2 3.0 05 21 1945 07 51 00 36.6 90.2 0 4 3.8 04 06 1946 00 00 00 35.2 84.9 0 4 3.8 11 07 1946 20 43 20 36.0 90.7 0 2- 3 3.2 05 06 1947 21 27 00 46.1 103.6 0 4 06 1947 01 27 00 46.1 103.6 0 4 0 0 00 00 35.2 84.9 0 4- 5 4.0 06 30 1947 04 23 53 38.4 90.2 40000 6 4.7 08 10 1947 01 46 48 42.0 85.0 18000 4- 5 4.0 01 15 1948 17 40 00 43.1 89.7 0 4 3.9 01 15 1948 00 00 00 31.9 92.6 0 4- 5 4.0 01 15 1948 00 00 00 41.7 83.6 0 3 3.4 02 10 1948 00 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 00 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 04 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 04 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 04 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 04 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 04 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 00 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 00 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 00 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 00 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 00 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 00 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 00 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 00 00 00 36.4 84.1 0 5- 6 4.5 04 20 1950 10 37 00 37.7 92.7 14000 5 4.2 05 05 05 05 05 05 05 05 05 05 05 05 05	11	16	1944	19	35	00	45.7	A7.1		0	2- 3		
03 28 1945 01 45 58 38.6 90.2 8000 3 3.4 05 18 1945 14 26 00 45.7 87.1 0 43.8 04 06 1946 00 00 00 35.2 84.9 0 4 3.8 10 26 1946 20 37 00 48.1 103.6 0 4 3.8 11 07 1946 20 43 20 36.0 90.7 0 2- 3 3.2 06 30 1947 04 23 53 38.4 90.2 40000 6 4.7 08 10 1947 01 46 48 42.0 85.0 18000 6 4.7 09 20 1947 21 30 00 31.9 92.6	12	10	1944	11	00	00	45.7	87.1		0	4	3.8	
05 21 1945 07 51 00 36.6 90.2 0 4 3.8 04 06 1946 00 00 00 35.2 84.9 0 4 3.8 10 26 1946 20 37 00 46.1 103.6 11 07 1946 20 43 20 38.0 90.7 0 2- 3 3.2 05 06 1947 21 27 00 43.0 87.9 8000 4- 5 4.0 08 30 1947 01 46 48 42.0 85.0 18000 6 4.7 08 10 1947 01 46 48 42.0 85.0 18000 6 4.7 09 20 1947 21 30 00 31.9 92.6 0 4- 5 4.0 01 15 1948 17 40 00 43.1 89.7 0 4 3.9 01 18 1948 00 00 00 44.7 83.6 0 3 3.4 02 10 1948 00 00 00 44.7 83.6 0 3 3.4 02 10 1948 00 00 00 44.7 83.6 0 3 3.4 02 10 1948 00 00 00 00 36.4 84.1 0 5- 6 4.5 04 20 1948 14 17 00 41.7 91.8 0 4 3.8 08 11 1949 16 32 00 36.6 90.3 0 2- 3 3.2 08 26 1949 00 00 00 03 35.8 84.0 0 2- 3 3.2 09 1950 13 24 00 37.7 92.7 14000 5 4.2 02 1951 08 00 00 00 35.8 84.0 0 4 3.8 09 20 1951 08 32 40 03 35.5 97.1 0 4 3.8 09 20 1951 08 00 00 00 41.6 81.4 0 2 3.0 0 10 17 1952 22 21 00 40.2 88.5 0 3 3.4 0 2 2 1951 04 00 00 44.6 81.4 0 2 3.0 0 10 17 1952 22 21 00 40.2 88.5 0 3 3.4 0 2 2 1951 04 00 00 44.6 81.4 0 2 3.0 0 10 17 1952 22 21 00 40.2 88.5 0 3 3.4 0 2 2 1952 09 38 06 39.7 82.1 13000 6 4.7 10 17 1952 15 48 00 30.1 93.7 0 4 3.8 0 5 07 1953 23 32 00 39.7 82.1 13000 6 4.7 10 17 1952 15 48 00 30.1 93.7 0 4 3.8 0 5 07 1953 23 32 00 39.7 82.1 13000 6 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4 3.8 0 5 07 1953 23 32 00 39.7 82.1 13000 6 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4 3.8 0 5 07 1953 20 00 00 00 41.6 81.4 0 2 3.0 0 4 3.8 0 5 07 1953 20 00 00 00 44.6 81.4 0 2 3.0 0 4 3.8 0 5 07 1953 23 32 00 39.7 82.1 10 0 4 3.8 0 6 39.7 82.1 10 0 4 3.8 0 6 39.7 82.1 10 0 4 3.8 0 6 39.7 82.1 10 0 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4 3.8 0 10 2 1955 06 00 00 47.3 88.4 0 4 3.8 0 10 2 1955 06 25 00 35.8 84.0 0 4 3.8 0 10 2 1955 06 25 00 35.8 84.0 0 4 3.8 0 10 2 1955 06 25 00 36.0 83.9 0 4 3.8 0 10 2 1955 06 25 00 35.8 84.0 0 0 4 3.8 0 10 2 1955 06 25 00 36.0 83.9 0 4 3.8 00 125 1955 06 25 00 36.0 83.9 0 4 3.8 0 125 1955 06 25 00 36.0 83.9 0 4 3.8 0 125 1955 00 37 00 30.0 14.5 80.0 00 00 47.1 88.6 0 5 4.2 0 125 1955 00 37 00 30.6 104.5 0 0 4 3.8 0 125 1955 00 37	03	28	1945	01	45			90.2	8			3.4	
04 06 1946 00 00 00 35.2 84.9 0 4 3.8 10 26 1946 20 37 00 46.1 103.6 0 4 3.8 11 07 1946 20 43 20 38.0 90.7 0 2- 3 3.2 05 06 1947 21 27 00 43.0 87.9 8000 4- 5 4.0 06 30 1947 04 23 53 38.4 90.2 40000 6 4.7 08 10 1947 04 26 48 42.0 85.0 180000 6 4.7 09 20 1947 21 30 00 31.9 92.6 0 4- 5 4.0 01 15 1948 17 40 00 43.1 89.7 0 4 3.9 01 18 1948 00 00 00 31.9 92.6 0 4- 5 4.0 01 15 1948 17 40 00 43.1 89.7 0 4 3.9 01 18 1948 00 00 00 34.7 83.6 G 3 3.4 02 10 1948 00 00 40 36.4 84.1 0 5- 6 4.5 04 20 1948 14 17 00 41.7 91.8 0 4 3.8 08 11 1949 16 32 00 36.6 90.3 0 2- 3 3.2 08 26 1949 00 00 00 38.6 90.7 0 3 3.4 02 00 1949 16 32 00 37.7 92.7 14000 5 4.2 02 15 1950 10 37 00 37.7 92.7 14000 5 4.2 02 15 1950 10 37 00 37.7 92.7 14000 4 5 4.0 03 20 1951 02 38 00 38.7 89.9 3000 4- 5 4.0 03 20 1951 02 38 00 38.7 89.9 3000 4- 5 4.0 04 3.8 09 20 1951 02 38 00 38.7 89.9 3000 4- 5 4.0 04 3.8 09 20 1951 02 38 00 38.7 89.9 3000 4 3.8 00 10 7 1952 22 21 00 40.2 88.5 0 3 3.4 0 2 3.0 12 22 1951 04 00 00 41.6 81.4 0 2 3.0 12 22 1951 04 00 00 44.6 81.4 0 2 3.0 12 22 1951 04 00 00 44.6 81.4 0 2 3.0 12 22 1951 04 00 00 44.6 81.4 0 2 3.0 12 22 1951 04 00 00 44.6 81.4 0 2 3.0 04 3.8 05 07 1953 23 32 00 39.7 82.1 13000 6 4.7 10 17 1952 15 48 00 30.1 93.7 13000 6 4.7 11 10 1953 15 48 00 30.1 93.7 12 04 3.8 05 07 1953 23 32 00 39.7 82.1 0 4 3.8 05 07 1953 23 32 00 39.8 82.1 0 4 3.8 05 07 1953 23 32 00 39.7 82.1 0 4 3.8 05 07 1953 23 32 00 39.7 82.1 0 4 3.8 05 07 1953 23 32 00 39.7 82.1 0 4 3.8 05 07 1953 23 32 00 39.7 82.1 0 4 3.8 05 07 1953 23 32 00 37.7 82.1 0 4 3.8 05 07 1953 23 32 00 30.1 93.7 11 10 1953 15 45 00 00 00 41.7 83.6 0 4 3.8 01 02 1955 20 00 00 00 47.3 88.4 0 4 3.8 01 02 1955 20 00 00 00 47.3 88.4 0 4 3.8 01 02 1955 20 00 00 00 47.3 88.4 0 4 3.8 01 02 1955 20 00 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 07 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 07 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 07 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 07 00 37 08 6 104.5 0 4 3.8 01 27 1955 07 00 37 00 30.6 104.5 0 4 3.8 01 27 1955 00 37 00 37 00 30.6 104.5 0 4 3.8 01 27	05	18	1945	14	26	00	45.7				2	3.0	
10 26 1946 20 37 00 48.1 103.6 0 4 3.8 11 07 1946 20 43 20 38.0 90.7 0 2-3 3.2 05 06 1947 21 27 00 43.0 87.9 8000 4-5 4.0 06 30 1947 04 23 53 38.4 90.2 40000 6 4.7 08 10 1947 01 46 48 42.0 85.0 18000C 6 4.7 09 20 1947 21 30 00 31.9 92.6 0 4-5 4.0 01 15 1948 17 40 00 43.1 89.7 0 4 3.9 01 18 1948 00 00 00 41.7 83.6 C 3 3.4 02 10 1948 00 00 00 36.4 84.1 0 5-6 4.5 04 20 1948 00 04 400 36.4 84.1 0 5-6 4.5 04 20 1948 14 17 00 41.7 91.8 0 4 3.8 08 11 1949 16 32 00 36.6 90.3 U 2-3 3.2 08 26 1949 00 00 00 37.3 8.6 90.7 0 3 3.4 02 15 1950 10 37 00 37.7 92.7 14000 5 5 4.2 03 20 1951 02 38 00 36.6 90.7 0 3 3.4 02 15 1950 10 37 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.7 89.9 3000 4 3.8 12 07 1952 00 00 00 00 41.6 81.4 0 2 3.0 01 07 1952 22 21 00 40.2 88.5 0 3 3.4 02 2 3.0 01 07 1952 22 21 00 40.2 88.5 0 3 3.4 02 2 3.0 01 07 1952 22 21 00 40.2 88.5 0 3 3.4 00 30.1 93.7 0 4 3.8 05 05 1953 00 00 00 00 41.6 81.4 0 2 3.0 01 07 1952 22 21 00 40.2 88.5 0 3 3.4 06 20 1955 00 30 00 00 37.3 83.2 0 4 3.8 05 05 1953 00 00 00 00 41.6 81.4 0 2 3.0 01 07 1952 20 00 00 00 41.7 83.6 0 4 3.8 09 11 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1955 10 00 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 00 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 00 00 00 47.1 88.6 0 5 4.2 01 12 1955 00 37 00 37 00 30.6 104.5 0 4 3.8 01 25 1955 00 37 00 37 00 30.6 104.5 0 4 3.8 01 25 1955 00 37 00 30.6 104.5 0 4 3.8 01 25 1955 00 37 00 37 00 30.6 104.5 0 4 3.	05	21	1945	07	51	00	36.6	90.2		0	4		
10 26 1946 20 37 00 48.1 103.6 0 4 3.8 11 07 1946 20 43 20 38.0 90.7 0 2-3 3.2 05 06 1947 21 27 00 43.0 87.9 8000 4-5 4.0 06 30 1947 04 23 53 38.4 90.2 40000 6 4.7 08 10 1947 01 46 48 42.0 85.0 18000C 6 4.7 09 20 1947 21 30 00 31.9 92.6 0 4-5 4.0 01 15 1948 17 40 00 43.1 89.7 0 4 3.9 01 18 1948 00 00 00 41.7 83.6 C 3 3.4 02 10 1948 00 00 00 36.4 84.1 0 5-6 4.5 04 20 1948 00 04 400 36.4 84.1 0 5-6 4.5 04 20 1948 14 17 00 41.7 91.8 0 4 3.8 08 11 1949 16 32 00 36.6 90.3 U 2-3 3.2 08 26 1949 00 00 00 37.3 8.6 90.7 0 3 3.4 02 15 1950 10 37 00 37.7 92.7 14000 5 5 4.2 03 20 1951 02 38 00 36.6 90.7 0 3 3.4 02 15 1950 10 37 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.8 84.0 0 4 3.8 09 20 1951 02 38 00 35.7 89.9 3000 4 3.8 12 07 1952 00 00 00 00 41.6 81.4 0 2 3.0 01 07 1952 22 21 00 40.2 88.5 0 3 3.4 02 2 3.0 01 07 1952 22 21 00 40.2 88.5 0 3 3.4 02 2 3.0 01 07 1952 22 21 00 40.2 88.5 0 3 3.4 00 30.1 93.7 0 4 3.8 05 05 1953 00 00 00 00 41.6 81.4 0 2 3.0 01 07 1952 22 21 00 40.2 88.5 0 3 3.4 06 20 1955 00 30 00 00 37.3 83.2 0 4 3.8 05 05 1953 00 00 00 00 41.6 81.4 0 2 3.0 01 07 1952 20 00 00 00 41.7 83.6 0 4 3.8 09 11 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1955 10 00 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 00 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 00 00 00 47.1 88.6 0 5 4.2 01 12 1955 00 37 00 37 00 30.6 104.5 0 4 3.8 01 25 1955 00 37 00 37 00 30.6 104.5 0 4 3.8 01 25 1955 00 37 00 30.6 104.5 0 4 3.8 01 25 1955 00 37 00 37 00 30.6 104.5 0 4 3.	04	06	1946	00	00	00	35.2	84.9		0		3.8	
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01 15 1948 17 40 00 43.1 A9.7 0 4 3.9 01 18 1948 00 00 00 41.7 83.6 C 3 3.4 02 10 1948 00 00 00 36.4 84.1 0 5-6 4.5 04 20 1948 14 17 00 41.7 91.8 0 4 3.8 08 11 1949 16 32 00 36.6 90.3 U 2-3 3.2 08 26 1949 00 00 00 03 86.6 90.3 U 2-3 3.2 08 26 1949 00 00 00 38.6 90.7 U 3 3.4 02 08 1950 10 37 00 37.7 92.7 14000 5 4.2 02 15 1950 10 05 00 46.1 95.2 3000 4-5 4.0 03 20 1950 13 24 00 33.5 97.1 U 4 3.8 09 20 1951 02 38 00 36.8 84.0 U 4 3.8 09 20 1951 02 38 00 36.7 89.9 3000 4 3.8 09 20 1951 08 32 00 41.6 81.4 U 250 4 3.8 12 07 1951 00 00 00 41.6 81.4 U 250 4 3.8 12 07 1951 00 00 00 41.6 81.4 U 2 3.0 01 07 1952 22 21 00 40.2 88.5 U 2 3.0 0 4 3.8 05 05 1953 00 00 00 43.8 82.1 13000 6 4.7 10 17 1952 15 48 00 30.1 93.7 U 4 3.8 05 07 1953 00 00 00 43.8 82.1 13000 6 4.7 10 17 1953 23 32 00 39.7 82.1 13000 6 4.7 11 10 1953 18 26 28 38.8 90.1 15000 3 4.7 11 10 1953 15 45 00 36.6 83.7 U 4 3.8 06 12 1953 00 00 00 00 37.3 83.2 U 4 3.8 06 12 1953 00 00 00 07 37.3 83.2 U 4 3.8 06 12 1953 00 00 00 07 37.3 83.2 U 4 3.8 06 12 1953 00 00 00 07 37.3 83.2 U 4 3.8 06 12 1953 00 00 00 07 37.3 83.2 U 4 3.8 06 12 1953 00 00 00 07 47.1 88.6 U 4 3.8 01 05 1955 21 00 00 47.3 88.4 U 4 3.8 01 05 1955 21 00 00 47.3 88.4 U 4 3.8 01 05 1955 20 00 00 47.1 88.6 U 5 4.2 01 12 1955 06 07 00 47.1 88.6 U 5 4.2 01 12 1955 06 07 07 47.3 88.4 U 4 3.8 U 4 3.8 01 07 1955 06 07 00 47.1 88.6 U 5 4.2 01 12 1955 06 07 07 07 47.3 88.4 U 4 3.8 U	09	20	1947	21	30	00	31.9	92.6		0	4- 5	4.0	
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06 12 1953 00 00 00 41.7 83.6 0 43.8 09 11 1953 18 26 28 38.8 90.1 15000 34.7 11 10 1953 15 45 00 36.0 83.9 0 43.8 12 31 1953 00 00 00 73.8 83.2 0 43.8 01 02 1954 03 23 00 36.6 83.7 0 64.7 01 05 1955 20 00 00 47.3 88.4 0 43.8 01 07 1955 05 00 00 47.1 88.6 0 54.2 01 07 1955 06 00 00 47.1 88.6 0 54.2 01 12 1955 20 35.8 84.0 0 43.8 01 25 1955 20 35.8 84.0 0 43.8 01 25 <td>05</td> <td>05</td> <td></td> <td>00</td> <td></td> <td>00</td> <td>39.8</td> <td>82.1</td> <td></td> <td>0</td> <td></td> <td></td> <td></td>	05	05		00		00	39.8	82.1		0			
09 11 1953 18 26 28 38.8 9c.1 15000 34.7 11 10 1953 15 45 00 36.0 83.9 0 43.8 12 31 1953 00 00 00 37.3 83.2 0 43.8 01 02 1954 03 23 00 36.6 83.7 0 64.7 01 05 1955 20 00 00 47.3 88.4 0 43.8 01 07 1955 05 00 00 47.1 88.6 0 54.2 01 07 1955 06 00 00 47.1 88.6 0 54.2 01 12 1955 06 25 00 35.8 84.0 0 43.8 01 25 1955 20 34 03.6 83.9 0 43.8 01 25 1955 20 37 00 36.0 83.9 0 43.8 02 01 1955 14 45 00 30.4 89.1 0 54.2	05	07	1953	23	32		39.7	82.1		0			
11 10 1953 15 45 00 36.0 83.9 0 4 3.8 12 31 1953 00 00 00 37.3 83.2 0 4 3.8 01 02 1954 03 23 00 36.6 83.7 0 6 4.7 01 05 1955 20 00 00 47.3 88.4 0 4 3.8 01 07 1955 05 00 00 47.3 88.4 0 4 3.8 01 07 1955 05 00 00 47.1 88.6 0 5 4.2 01 07 1955 06 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 25 00 35.8 84.0 0 4 3.8 01 25 1955 20 34 00 36.0 83.9 0 4 3.8 01 27 1955 00 37 00 30.6 104.5 0 4 3.8 02 01 1955 14 45 00 30.4 89.1 0 5 4.2	06	12		00			41.7	83.6		0		3.8	
12 31 1953 00 00 00 37.3 83.2 0 4 3.8 01 02 1954 03 23 00 36.6 83.7 0 6 4.7 01 05 1955 20 00 00 47.3 88.4 0 4 3.8 01 07 1955 21 00 00 47.1 88.6 0 5 4.2 01 07 1955 06 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 25 00 35.8 84.0 0 4 3.8 01 25 1955 20 34 00 36.0 83.9 0 4 3.8 01 27 1955 00 37 00 30.6 104.5 0 4 3.8 01 27 1955 14 45 00 30.4 89.1 0 5 4.2							38.8		150				
01 02 1954 03 23 00 36.6 83.7 0 6 4.7 01 05 1955 20 00 00 47.3 88.4 0 4 3.8 01 05 1955 21 00 00 47.3 88.4 0 4 3.8 01 07 1955 05 00 00 47.1 88.6 0 5 4.2 01 07 1955 06 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 25 00 35.8 84.0 0 4 3.8 01 25 1955 20 34 00 36.0 83.9 0 4 3.8 01 27 1955 00 37 00 30.6 104.5 0 4 3.8 02 01 1955 14 45 00 30.4 89.1 0 5 4.2							36.0	83.9					
01 05 1955 20 00 00 47.3 88.4 0 4 3.8 01 05 1955 21 00 00 47.3 88.4 0 4 3.8 01 07 1955 05 00 00 47.1 88.6 0 5 4.2 01 07 1955 06 25 00 35.8 84.0 0 4 3.8 01 25 1955 20 34 00 36.0 83.9 0 4 3.8 01 27 1955 00 37 00 30.6 104.5 0 4 3.8 02 01 1955 14 45 00 30.4 89.1 0 5 4.2	12						37.3	83.2					
01 05 1955 21 00 00 47.3 88.4 0 4 3.8 01 07 1955 05 00 00 47.1 88.6 0 5 4.2 01 07 1955 06 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 25 00 35.8 84.0 0 4 3.8 01 25 1955 20 34 00 36.0 83.9 0 4 3.8 01 25 1955 20 37 00 30.6 104.5 0 4 3.8 02 01 1955 14 45 00 30.4 89.1 0 5 4.2					-		36.6						
01 07 1955 05 00 00 47.1 88.6 0 5 4.2 01 07 1955 06 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 25 00 35.8 84.0 0 4 3.8 01 25 1955 20 34 00 36.0 83.9 0 4 3.8 01 27 1955 00 37 00 30.6 104.5 0 4 3.8 02 01 1955 14 45 00 30.4 89.1 0 5 4.2							47.3						
01 07 1955 06 00 00 47.1 88.6 0 5 4.2 01 12 1955 06 25 00 35.8 84.0 0 4 3.8 01 25 1955 20 34 00 36.0 83.9 0 4 3.8 01 27 1955 00 37 00 30.6 104.5 0 4 3.8 02 01 1955 14 45 00 30.4 89.1 0 5 4.2			1955										
01 12 1955 06 25 00 35.8 84.0 0 4 3.8 01 25 1955 20 34 00 36.0 83.9 0 4 3.8 01 27 1955 00 37 00 30.6 104.5 0 4 3.8 02 01 1955 14 45 00 30.4 89.1 0 5 4.2													
01 25 1955 20 34 00 36.0 83.9 0 4 3.8 01 27 1955 00 37 00 30.6 104.5 0 4 3.8 02 01 1955 14 45 00 30.4 89.1 0 5 4.2				1000							5		
01 27 1955 00 37 00 30.6 104.5 0 4 3.8 02 01 1955 14 45 00 30.4 89.1 0 5 4.2					-		35.8						
02 01 1955 14 45 00 30.4 89.1 0 5 4.2				7.0									
05 26 1955 18 09 00 41.5 81.7 0 5 3.8													
	05	26	1955	18	09	00	41.5	81.7		Ü	5	3.8	

(Continued)

(Sheet 6 of 8)

Table 10 (Continued)

1	DATI		OT	(UT)	LAT	LON	FELT AREA	1	10	MB	MS
06	29	1955	01	16	00	41.5	81.7	0		5	3.8	
01	08	1956	00	35	00	29.3	94.8	0		4	3.8	
03	13	1956	15	15	00	40.5	90.4	5000		4	3.8	
07	18	1956	21	30	00	43.6	97.7	0		4	3.8	
07	18	1956	23	00	00	43.6	87.7	0		4	3.8	
09	09	1956	22	45	00	35.8	86.7	400		4	3.8	
10	13	1956	00	00	00	42.9	87.9	0		4	3.8	
10	30	1956	10	36	00	36.2	95.9	25000		7	4.7	
01	08	1957	16	00	00	43.5	88.8	0	3-	4	3.6	
01	25	1957	18	15	00	36.6	83.7	0		6	4.0	
03	19	1957	16	38	00	32.6	94.7	47000		5	4.3	
03	19	1957	17	41	00	32.6	94.7	0		Ü	3.0	
03	19	1957	22	36	00	32.6	94.7	0		U	3.0	
03	19	1957	22	45	00	32.6	94.7	U		0	3.0	
06	23	1957	06	34	18	36.5	84.5	C		5	4.2	
06	29	1957	00	00	00	42.9	81.3	U		4	3.8	
07	23	1957	13	03	00	36.7	83.8	0		3	3.4	
05	01	1958	22	47	00	41.5	81.7	C	4-	5	4.0	
10	23	1958	02	29	47	37.5	82.5	0		0	3.0	
11	06	1958	23	08	00	29.9	90.1	0		4	3.8	
11	19	1958	18	15	00	30.5	91.2	800		5	4.2	
01	06	1959	15	07	00	38.7	90.3	0		3	3.4	
06	13	1959	01	00	00	35.4	84.3	0		4	3.8	
08	12	1959	18	06	07	35.0	87.0	7000		6	4.7	
10	15	1959	15	45	00	29.8	93.1	6500		4	3.8	
04	15	1960	10	10	10	35.8	84.0	3400		5	4.2	
04	13	1961	21	1.4	57	39.9	100.0	3600		5	4.2	
12	25	1961	12	20	03	39.1	94.6	0		4	3.6	
12	25	1961	12	58	21	39.1	94.6	40000		5	3.8	
12	05	1963	06	51	02	37.2	87.0	0	2-	3	3.2	
12	15	1963	05	35	00	37.2	87.1	0		3	3.4	
05	18	1964	09	31	10	34.8	85.5	0		5	4.2	
04	24	1964	01	24	55	31.5	93.8	0		4	3.8	
04	24	1964	07	33	53	31.6	93.8	0		4	4.0	
04	24	1964	07	47	18	31.3	93.8	0		U	3.3	
04	24	1964	12	0.7	07	31.3	03.8	0		0	3.2	
04	24	1964	12	54	17	31.3	93.8	0		0	3.0	
04	26	1964	03	24	50	31.3	93.8	0		0	3.3	
04	27	1964	21	50	27	31.3	93.8	0		0	3.2	
04	28	1964	00	24	07	31.5	93.8	0		0	3.1	
04	28	1964	00	30	46	31.5	93.8	600		4	4.0	
04	28	1964	21	18	35	31.2	93.9	0		5	4.0	
04	30	1964	21	30	00	31.2	94.0	0		0	3.0	
05	02	1964	06	34	54	31.3	93.8	Ü		0	3.2	
05	03	1964	03	24	12	31.3	93.8	0		U	3.0	
05	07	1964	20	01	39	31.2	94.0	0		6		
06	03	1964	02	27	24	31.5	93.9	0	,	4	3.1	
06	03	1964	09	37	00	31.0	94.0	Ü	3-	4	3.6	
07	28	1964	00	35	31	36.0	83.9	Ö		5	3.0	
08	16	1964	11	30		31.4	93.8	0		0	3.0	
10	10	1964	90	30	00	47.4	89.8	U		U	3.0	

(Continued)

(Sheet 7 of 8)

Table 10 (Concluded)

DATE														
10 13 1964 16 30 00 36.0 83.9 0 2-3 3.2 02 14 1965 20 03 20 36.9 93.3 0 3.0 03.0 1965 21 08 50 37.4 91.1 0 3 4.1 08 30 1965 22 04 51 37.4 91.1 0 0 3.5 12 09 1965 22 04 51 37.4 91.1 0 0 3.5 0 3.0 0 24 1966 23 45 00 30.0 94.0 0 0 3.5 0 0 26 1966 11 59 44 44.3 104.3 3000 6 3.1 08 24 1966 00 00 00 35.8 84.0 0 4 3.8 09 28 1966 00 00 00 35.8 84.0 0 4 3.8 12 06 1966 08 00 47 38.9 92.8 0 0 3.0 0 3.0 0 22 1967 06 30 00 42.7 84.6 0 4 3.8 12 06 1966 08 00 47 38.9 92.8 0 0 3.0 0 3.0 0 22 1967 06 30 00 42.7 84.6 0 4 3.8 10 14 1968 14 42 54 34.0 96.8 0 5 3.5 10 31 1968 16 00 00 38 38 76.8 0 5 3.5 10 31 1968 16 00 00 38.3 85.8 0 5 3.5 10 31 1968 16 00 00 38.3 85.8 0 5 3.5 10 31 1968 16 00 00 38.3 85.8 0 5 3.5 10 31 1969 21 51 09 36.1 83.7 50000 5 4.3 0 7 13 1969 21 51 09 36.1 83.7 50000 5 4.3 0 7 13 1969 21 51 09 36.1 83.7 50000 5 4.3 0 7 13 1969 11 15 00 36.0 83.9 0 2 3.0 0 3.4 3.8 12 0 1969 01 00 09 37.4 81.0 250000 6 4.7 0 2 3.0 0 2 06 1970 04 22 00 37.9 90.6 0 2 3.0 0 2 3.0 0 2 2 3.0 0 2 2 3.0 0 3 1970 00 02 02 37.9 90.6 0 2 3.2 0 2 3.0 0 3 1970 09 39 11 37.9 90.6 0 2 3.0 0 3.0 0 3.0 0 3 10 1970 09 39 11 37.9 90.6 0 2 3.0 0 3.0 0 3.0 0 3 14 1971 17 27 51 33.1 88.1 0 0 3.0 3.0 0 3.7 0 3 1970 10 5 04 29 33.1 88.1 0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0 3.0 0	1	DAT	E	OT	(UT)		LUN	FELT	AREA	1	10	MB	MS
02 14 1965 20	10	10	1964	11	30	00	47.3	90.3					3.0	
03 06 1965 21 08 50 37.4 91.1 0 3 4.1 08 30 1965 05 17 38 32.1 102.3 0 4 3.5 12 09 1965 22 04 51 37.4 91.1 0 0 3.5 13 24 1966 23 45 00 30.0 94.0 0 0 3.0 06 26 1966 11 59 44 44.3 104.3 3000 6 3.1 08 14 1966 00 00 00 03 55.8 84.0 09 28 1966 00 00 00 35.8 84.0 09 28 1966 00 00 00 37.8 84.0 09 28 1966 00 00 00 37.8 84.0 09 28 1966 00 00 47 38.9 92.8 0 0 3.8 12 06 1966 08 00 47 38.9 92.8 0 0 3.8 12 06 1966 08 00 42.7 84.6 0 4 3.8 12 06 1966 08 00 42.7 84.6 0 4 3.8 12 01 14 1968 14 42 54 34.0 96.8 0 6 3.5 10 31 1968 16 00 00 38.3 85.8 0 5 3.5 10 31 1968 16 00 00 38.3 85.8 0 5 3.0 17 13 1969 21 51 09 36.1 83.7 50000 5 4.3 17 14 1969 11 15 00 36.0 83.9 0 2 3.0 17 24 1969 18 10 00 36.0 83.9 0 2 3.0 17 24 1969 18 10 00 36.0 83.9 0 3 3.4 12 00 1969 01 00 09 37.4 81.0 250000 6 4.7 12 00 1969 01 00 09 37.4 81.0 250000 6 4.7 12 01 1969 10 00 09 37.9 90.6 0 2 3.0 12 06 1970 04 28 00 37.9 90.6 0 2 3.0 13 1970 08 48 51 37.9 90.6 0 2 3.0 13 1971 04 53 02 37.9 90.6 0 2 3.0 13 1971 05 04 28 32.8 88.3 0 0 3.5 13 16 1971 02 37 28 32.8 88.3 0 0 3.5 13 16 1971 02 37 28 32.8 88.3 0 0 3.5 13 17 1971 17 27 51 33.1 87.9 0 0 3.5 14 1971 17 27 51 33.1 87.9 0 0 3.5 15 17 1971 10 5 04 29 37.1 83.2 0 0 3.0 17 30 1970 10 4 29 33.1 88.1 0 0 3.5 10 31 1971 14 53 49 31.7 103.1 0 4 3.4 10 10 1771 05 04 29 37.4 81.6 0 0 3.5 10 31 1971 14 53 49 31.7 103.1 0 4 3.4 10 10 1771 05 04 29 37.4 81.6 0 0 3.0 17 30 1970 10 45 51 37.4 81.6 0 0 3.0 17 31 1971 14 53 49 31.7 103.1 0 4 3.4 10 10 1771 05 05 11 37.4 87.3 0 0 3.5 10 30 1973 22 58 01 37.4 87.3 0 0 3.5 11 30 1973 22 58 01 37.4 87.3 0 0 0 3.2 11 30 1973 22 58 01 37.4 87.3 0 0 0 3.2 11 30 1973 22 58 01 37.4 87.3 0 0 0 3.2 11 30 1973 22 58 01 37.4 87.3 0 0 0 3.2 11 30 1973 22 58 01 37.4 87.3 0 0 0 3.2 11 30 1973 22 58 01 37.4 87.3 0 0 0 3.2 11 30 1973 27 48 41 35.8 84.0 0 0 6 3.6 12 10 1974 15 13 55 39.1 81.6 0 0 5 3.4 12 10 1975 11 50 00 33.5 88.0 0 0 0 3.2 13 10 1975 11 50 00 33.5 88.0 0 0 0 3.2	10	13	1964	16	30	00	36.0	83.9		C	2-	3	3.2	
03 06 1965 21 08 50 37.4 91.1 0 3 4.1 08 30 1965 05 17 38 32.1 102.3 0 4 3.5 12 09 1965 22 04 51 37.4 91.1 0 0 3.5 03 24 1966 23 45 00 30.0 94.0 0 0 3.0 06 26 1966 11 59 44 44.3 104.3 3000 6 3.1 08 14 1966 15 25 52 31.7 103.1 50000 6 4.3 08 24 1966 00 00 00 35.8 84.0 0 4 3.8 09 28 1966 00 00 00 35.8 84.0 0 4 3.8 12 06 1966 08 00 47 38.9 92.8 0 3.0 02 02 1967 06 30 00 42.7 84.6 0 4 3.8 04 08 1967 05 40 32 39.6 82.5 10000 5 4.2 10 14 1968 14 42 54 34.0 96.8 0 6 3.5 10 31 1968 00 00 00 43.0 83.0 0 5 4.2 10 14 1968 16 00 00 43.0 83.0 0 5 4.3 11 1968 16 00 00 36.3 83.0 0 5 3.0 07 13 1969 21 51 09 36.1 83.7 50000 5 4.3 07 14 1969 11 15 00 36.0 83.9 0 2 3.0 07 24 1969 18 10 00 36.0 83.9 0 3 3.4 11 20 1969 01 00 09 37.4 81.0 250000 6 4.7 02 03 1970 00 00 00 31.0 97.0 0 4 3.8 02 06 1970 04 28 00 37.9 90.6 0 2 3.0 02 06 1970 04 28 00 37.9 90.6 0 2 3.0 03 14 1971 17 27 51 33.1 87.9 90.6 03 19 1971 23 11 42 37.1 83.2 0 0 3.0 03 16 1971 02 37 28 32.8 88.3 0 0 3.7 03 14 1971 17 27 51 33.1 87.9 0 0 3.5 03 16 1971 02 37 28 32.8 88.3 0 0 3.5 03 16 1971 05 04 29 37.4 81.6 0 0 3.5 03 16 1971 07 25 55 31.7 103.1 0 4 3.8 02 19 1971 14 53 22 32.8 88.3 0 0 3.5 03 16 1971 07 14 53 13 7.4 87.9 0 0 3.0 04 01 1975 11 45 39 90.6 0 0 3.0 07 30 1970 08 48 51 37.0 82.2 0 0 3.0 07 31 1971 14 53 49 31.7 103.1 0 4 3.4 01 09 1972 23 24 29 37.4 81.6 0 0 3.0 07 31 1971 14 53 39 90.6 37.9 90.6 0 0 3.5 03 16 1971 07 14 55 37.4 81.6 0 0 3.0 07 30 1970 14 5 13 55 39.1 81.6 0 0 3.0 07 30 1973 22 58 01 37.4 87.3 0 0 0 3.2 01 1975 13 55 39.1 81.6 0 0 5 3.4 01 00 1975 23 21 31 39.0 82.4 0 0 3.3 01 1975 11 50 00 33.5 88.0 0 0 6 4.6	02	14	1965	20	03	20	36.9	93.3		0		0	3.0	
12 09 1965 22 04 51 37.4 91.1 0 0 3.5 03 24 1966 23 45 00 30.0 94.0 0 0 3.1 06 26 1966 11 59 44 44.3 104.3 3000 6 4.3 08 14 1966 15 25 52 31.7 103.1 50000 6 4.3 08 24 1966 00 00 00 355.8 84.0 0 4 3.8 09 28 1966 00 00 00 379.3 80.3 0 4 3.8 12 06 1966 08 00 47 38.9 92.8 0 3.0 12 06 1966 08 00 47 38.9 92.8 0 4 3.8 12 06 1966 08 00 47 38.9 92.8 0 4 3.8 12 06 1966 08 00 47 38.9 92.8 0 5 3.0 14 1968 14 42 54 34.0 96.8 0 6 3.5 10 31 1968 00 00 00 43.0 83.0 0 5 4.2 10 14 1968 16 00 00 43.0 83.0 0 5 4.2 11 1968 16 00 00 38.3 85.8 0 5 3.0 07 13 1969 21 51 09 36.1 83.7 50000 5 4.3 07 14 1969 11 15 00 36.0 83.9 0 2 3.0 07 24 1969 18 10 00 36.0 83.9 0 2 3.0 12 20 1969 01 00 09 37.4 81.0 250000 6 4.7 12 01 1969 01 00 09 37.4 81.0 250000 6 4.7 12 02 1969 01 00 09 37.9 90.6 0 2 3.0 12 02 1970 04 28 00 37.9 90.6 0 2 3.0 12 05 1970 04 53 02 37.9 90.6 0 2 3.0 13 1970 08 48 51 37.0 82.2 U 0 3.0 14 1971 05 05 31 37.9 90.6 0 2 3.0 08 11 1970 06 14 25 38.4 82.3 0 4 3.8 02 19 1971 23 11 42 37.1 83.2 0 0 3.0 08 11 1970 15 04 29 33.1 87.9 03 15 1971 14 53 22 32.8 88.3 0 0 3.5 03 16 1971 07 45 51 33.1 87.9 0 0 0 3.9 03 15 1971 14 53 49 31.7 103.1 0 3 3.0 04 01 1971 05 05 11 37.4 81.6 0 0 3.0 07 30 1970 07 48 41 35.8 88.3 0 0 3.5 07 31 1971 01 45 51 31.7 103.1 0 3 3.0 07 31 1971 01 45 34 9 31.7 103.1 0 3 3.0 07 31 1971 10 45 34 9 31.7 103.1 0 3.0 07 30 1973 22 56 01 37.4 81.6 0 0 3.0 07 30 1973 22 58 39 35.7 83.9 0 5 3.4 1 30 1973 22 56 01 37.4 87.3 0 0 3.0 07 30 1974 00 16 40 35.8 84.8 0 6 6 3.6 00 1974 00 16 40 35.8 84.8 0 6 6 3.6 00 1975 23 21 13 39.0 82.4 0 6 3.5 01 1975 11 50 00 33.5 88.0 0 0 3.3 01 1975 11 50 00 33.5 88.0 0 0 3.3	03	06	1965	21	08	50	37.4			0		3	4.1	
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11 30 1973 07 48 41 35.8 84.0 0 6 4.6 06 05 1974 00 16 40 36.6 84.8 0 6 3.6 10 20 1974 15 13 55 39.1 81.6 0 5 3.4 02 16 1975 23 21 31 39.0 82.4 0 0 3.3 03 01 1975 11 50 00 33.5 88.0 0 2 3.2		-					35 7			-				
06 05 1974 00 16 40 35.6 84.8 0 6 3.6 10 20 1974 15 13 55 39.1 81.6 0 5 3.4 02 16 1975 23 21 31 39.0 82.4 0 0 3.3 03 01 1975 11 50 00 33.5 88.0 0 2 3.2		-					35 A							
10 20 1974 15 13 55 39.1 81.6 0 5 3.4 02 16 1975 23 21 31 39.0 82.4 0 0 3.3 03 01 1975 11 50 00 33.5 88.0 0 2 3.2														
02 16 1975 23 21 31 39.0 82.4 0 0 3.3 03 01 1975 11 50 00 33.5 88.0 0 2 3.2		30.00	700		-									
03 01 1975 11 50 00 33.5 98.0 0 2 3.2														
		_								-				
00 24 19/3 11 11 00 30,/ 5/.0 0 4 4.3					_			100 (0.7)						
	00	24	14/5	11	1.	08	30.7	57.0				7	4.5	

(Sheet 8 of 8)

Practically this means that the earthquake must have a body-wave magnitude of about 5 or greater, which limits the applicability of the method to only a few central United States earthquakes.

29. The third method makes use of the fact that the period of the minimum in the spectrum of the Rayleigh-wave motion is a function of focal depth and of focal mechanism. Knowing the latter, one can find the former. Herrmann¹³ applied this technique to sixteen earthquakes in the central United States. The shallowest, an August, 1965 Illinois event, had a depth of only 1.5 km. The deepest, which also occurred in Illinois in November 1968, had a depth of 22 km. Seventy-five percent of the earthquakes studied had depths between 5 and 16 km. His study supports the conclusion, based on the observation of travel times of body waves at small epicentral distances, that the foci of central United States earthquakes generally lie in the upper twenty kilometers of the crust.

Frequency Content of Seismic Waves

30. Damaging ground motion generally is confined to the frequency range of 1 to 10 Hz, which corresponds to the natural or resonant frequencies of most man-made structures. Until the mid-1970's all of the seismographs operating in the central United States had natural frequencies of approximately 1 Hz or less, so they did not respond to the higher-frequency part of the damaging ground-motion spectrum. Thus there was little information on the amount of high-

frequency source motion or on its dissipation with increasing epicentral distance.

31. Since the mid-1970's strong-motion accelerographs and microearthquake-recording seismographs have been operating in the New Madrid seismic zone. The strong-motion instruments were triggered by three earthquakes: the 13 June 1975 event in southeast Missouri, the 25 March 1976 event of eastern Arkansas and an after-shock of the latter earthquake. The strong-motion records showed that 10-Hz waves could be observed as far away as 150 km¹⁴. Seismograms from the microearthquake array shown in Figure 1 showed 10-Hz waves as distant as 370 km for other earthquakes¹⁵. Thus both sets of data indicate that excitation of 10-Hz wave energy occurs and that attenuation is relatively low for 10-Hz waves in the central Mississippi valley.

Focal Mechanisms

32. Herrmann¹³ determined focal mechanisms for all the central United States earthquakes for which adequate data are available. He used the amplitude and phase spectra of long-period Rayleigh and Love waves and the P-wave first-motion data to infer the orientation of the fault plane, the type of faulting and the orientation of the pressure axes in those cases for which they were nearly horizontal. Twelve of the earthquakes were primarily of the strike-slip type. Two, in the St. Francois highlands of the Ozark uplift, indicated normal faulting.

One at the Ouachita mountain front in Arkansas and one in the Wabash valley of Illinois indicated reverse faulting. The pressure axes trended NE or E for most of the earthquakes having horizontal axes.

- 33. Herrmann and Canas¹⁶ found that the fault planes of three earthquakes occurring along the southwest branch of the New Madrid fault zone had the same strike as the 120-km trend of microearthquakes along this branch of the fault zone. They also found that a fault-plane solution obtained from a composite of P-wave motions from a number of microearthquakes along the fault gave a similar focal mechanism, which indicated oblique faulting with a component of right-lateral strike-slip faulting as well as some vertical movement.
- depth, is important if one wishes to compute synthetic seismograms or time histories of the ground motion at a particular site. In the central United States this capability at present exists only for the southwest branch of the New Madrid fault zone. This is the zone, however, which is capable of producing the largest earthquakes in the central and eastern United States. About 75 percent of the earthquakes studied by Herrmann¹³ had significant components of strike-slip motion, which means that the earthquakes generate a substantial amount of tangential SH ground motion. The possibility exists for making theoretical estimates for other regions as well, though not as precisely as for earthquakes in the New Madrid seismic zone.

Attenuation

- 35. Attenuation of ground motion results from two principal causes: the geometrical spreading of energy as the distance increases and a frictional or absorptive loss. The latter is referred to as anelastic attenuation.
- 36. Geometric attenuation is in general independent of wave frequency or wavelength. Anelastic attenuation varies with wave frequency, being greater for the higher frequency waves. Anelastic attenuation also varies with crustal geology for wave frequencies of interest in earthquake engineering. In the United States, for example, the absorption of 1 to 10 Hz waves is greater in the western than in the eastern United States.
- 37. Nuttli and Dwyer¹⁵ showed that the value of the specific dissipation factor, Q, for 1- to 10-Hz surface waves in the central United States is 1500. This corresponds to a coefficient of absorption of 0.0006 km⁻¹ for 1-Hz waves and 0.006 km⁻¹ for 10-Hz waves. Chouet et al¹⁷ found an average Q value of 200 for tectonic provinces, such as California and Japan. This corresponds to a coefficient of absorption of 0.0045 km⁻¹ for 1-Hz waves and 0.045 km⁻¹ for 10-Hz waves.

Ground-Motion Character

- 38. Differences in attenuation of seismic waves in the central and western United States lead to differences in the character of the ground motion, depending on the epicentral distance. They affect the amplitude, the frequency and the duration of the ground motion.
- 39. At very small distances, out to 10 km, there will be no essential difference in the character of the ground motion, because absorption is not important at such distances. At distances of 10 to 100 km, 1-Hz waves will have essentially the same amplitude and duration in the central and western United States for earthquakes of similar magnitude. But 10-Hz waves in the West will be ten times smaller at 100 km distance than in the central region. Thus a time history in the central region will be richer in the high frequencies than one in the western region, but the 1-Hz waves will be essentially the same.
- 40. At distances of greater than 100 km the 10-Hz wave motion rarely is seen in the West, whereas it will be observable in the central region. The amplitudes of 1-Hz waves in the West will be comparable to those of 10-Hz waves in the central United States. In the latter region, the 1-Hz waves will maintain relatively large amplitudes, and will be especially noticeable in long and tall structures (ten stories and greater).

- 41. In general, one can conclude that within the near-field region of earthquakes the time history of central and western United States earthquakes will be practically the same. But in the far-field region the amplitude and acceleration will be greater in the central United States than in the West. Duration will be greater also in the central region, but the difference will not be so large as for amplitudes and accelerations.
- 42. These observations of the attenuation of seismic energy indicate that the transmission medium in the central region can potentially propagate destructive ground motion to larger distances than in the western region. Such would be the case if the energetics of the seismic sources in the two regions are the same. Estimation of the source spectra of earthquakes by Street et al., 18 Street and Turcotte¹⁹ for eastern North America and by Chouet et al., 17 and Thatcher and Hanks²⁰ in the Western United States indicate substantial regional differences. In general, central United States earthquakes excite fewer higher frequencies than do western earthquakes for magnitudes less than 6.0. Larger eastern North American earthquakes seem to behave in the same manner as large earthquakes worldwide. This indicates that for design earthquakes having magnitudes, mb, less than 6.0 in the central region, the effects of efficient high frequency wave propagation may be mitigated by low excitation of those frequencies.

PART IV: REGIONAL IDENTIFICATION OF CREDIBLE EARTHQUAKES Methodology for Estimating Maximum-Magnitude Earthquakes

- 43. To specify the credible earthquake motion it is necessary to determine the maximum-magnitude earthquake for each seismic source region. Thus it is necessary to develop a methodology for determining the maximum-magnitude earthquake. In the central United States, where the location and extent of active faults are at best poorly known, one must rely principally on seismological rather than on geological data. The best available information is the catalog of earthquake activity. The problem is to find a procedure for estimating the maximum-magnitude earthquake from the data of the catalog.
- 44. There are two regions in the central and eastern United States where the maximum-magnitude earthquake can be presumed to have occurred in historic times. The first is the New Madrid region, where an earthquake of m_b = 7.5 occurred on 7 February 1812². The second is the Charleston, South Carolina region, where an earthquake of m_b = 6.6 to 6.9 occurred on 31 August 1886². A methodology is sought, then, which will give such magnitudes if these earthquakes are deleted from the catalog.
- 45. Figure 4 gives the cumulative magnitude-recurrence data and curve for New Madrid regions A and B, excluding the three major earthquakes of 1811-1812. The ordinate is the number of earthquakes

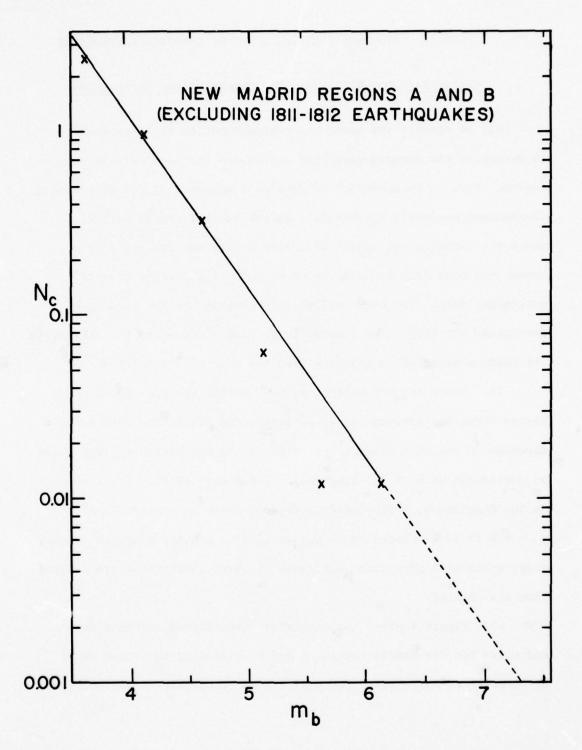


Figure 4. Cumulative magnitude-recurrence curve for New Madrid regions A and B, excluding the 1811-1812 earthquakes

per year equalling or exceeding the m_b value, which is the abscissa. For the smaller magnitudes the data of Tables 8 and 9 were examined for completeness, and the value of the number of earthquakes per year was derived only from the more recent years where the reporting of small-magnitude events is better than for the earlier years. The straight-line curve has a slope of 0.92, similar to that found by Nuttli⁴ for a 140-year set of data for the central Mississippi valley. If the curve is extrapolated to N_c =0.001 (a recurrence period of 1000 years) the corresponding m_b is 7.35, which is very close to the presumed maximum magnitude of 7.5 for the region.

- 46. Figure 5 shows the cumulative magnitude-recurrence data and curve for the Charleston, South Carolina region, excluding the 1886 earthquake. The data, which are taken from $Tarr^{21}$, are fitted by a straight line of slope 0.70. The extrapolation to N_c =0.001 indicates an earthquake with a recurrence period of 1000 years will have an m_b of 6.85. This is within the range of values 6.6 to 6.9 assigned to the maximum-magnitude earthquake².
- 47. The procedure, then, to estimate the maximum-magnitude earthquake for a seismic source region will be to extrapolate the recurrence curve to obtain the m_b associated with a 1000-year recurrence period. Because the data for the other source regions of the central United States will not cover as large a magnitude interval as for New Madrid or Charleston, the slope will not be so well defined, which will lead to large uncertainties in estimating the maximum-magnitude

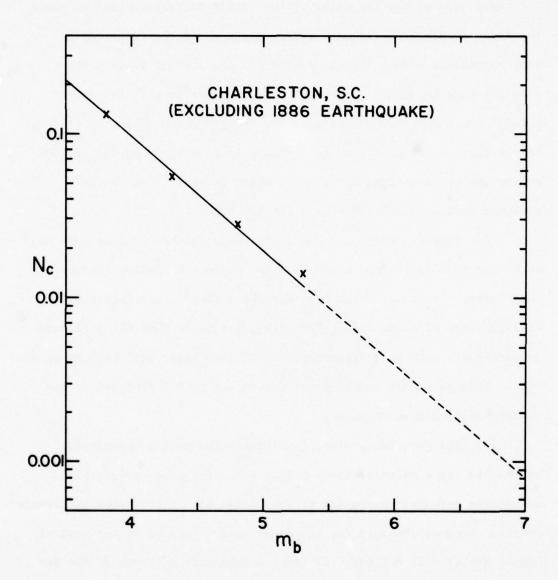


Figure 5. Cumulative magnitude-recurrence curve for the Charleston, South Carolina region, excluding the 1886 earthquake

earthquake. To avoid this problem the slope, for all central United States source regions, will be assumed to be 0.92, the value found for the central Mississippi valley⁴. The data will be fitted by the best straight line, in the sense of lease squares, which has a slope of 0.92. In this curve fitting procedure, the largest magnitude data point will be given one-half the weight of the other points.

- 48. The procedure described in paragraphs 45-47 does not take account of the area of the seismic source region. This is a short-coming, for it is obvious that if the source area is enlarged there will be more earthquakes included in it and the magnitude-recurrence curve will be displaced upward, which would imply an increase in the value of the maximum-magnitude earthquake. To avoid this paradox the value of $N_{\rm C}$ must be equalized to a particular source area. The problem is to find the value of the source area to be used for equalization. If the New Madrid region is enlarged to include the entire central Mississippi valley, the apparent maximum-magnitude earthquake has a value larger than 7.5. To bring it back to 7.5, it is found that it is necessary to equalize to a source area of 100,000 km². That is, all the value of $N_{\rm C}$ must be divided by the ratio of the actual area to 100,000 km². This equalized value of $N_{\rm C}$ will be called $N_{\rm C}$.
- 49. Although the data of source regions with areas larger than 100,000 km² must be equalized, it does not follow that a similar procedure should be used for data from areas of less than 100,000 km².

That is, a small source region will have a small fault length, which will limit the size of the maximum-magnitude earthquake. To enlarge the area to 100,000 km² would hypothetically enlarge the length of the fault zone, and thus make the maximum-magnitude estimate too large. Therefore, the recurrence data are not equalized for area if the source region has an area of less than 100,000 km².

Recurrence Equations and Maximum-Magnitude Earthquakes for Central United States Source Regions

50. For the central United States the magnitude-recurrence equation is assumed to have the form

$$log_{10} N_c' = a - 0.92 m_b$$

where N_c^{\prime} is the cumulative number of earthquakes of m_b or greater which occur in a 100,000 km² area in one year. If the source area is less than 100,000 km², N_c is the number of earthquakes of m_b or greater which occur in the source region in one year.

- 51. If the value of \underline{a} in the magnitude-recurrence equation is determined for a particular source region, the value of the maximum-magnitude earthquake, $m_{b,max}$, can be found by putting $N_c' = 0.001$. Thus, by specifying the slope of the magnitude-recurrence curve, $m_{b,max}$ becomes a linear function of the intercept \underline{a} .
- 52. Tables 11 through 20 present the ten-year activity rates and the cumulative activity rates per decade for each of the seismic source

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Table 11

TEN YEAR ACTIVITY RATES

SOURCE	REGION	ANNA, OHIO
ADEA -	7740E	VM2

85 6.35 35 6.85 0 0	6.85 7.35	7.35 7.85	SUM
0 0 0 0	7.35	7.85	DECADE
0 0	0	0	•
0 0	0		2
0 0		0	1
0 0	0	0	2
0 0	0	0	12
0 0	0	0	16
0 0	0	0	2
0 0	0	0	1
0 0	0	0	1
0 0	0	0	2
0 0	0	0	4
0 0	0	0	3
0 0	0	0	0
0 0	0	0	n
0 0	0	0	•
0 0	O	0	ō
0 0	0	0	0
0 0	0	Ö	0
0 0	0	0	47

YR/MB	2.85	3.35	3.65	4.35	4.85	5.35	5,85	6.35	6.85	7.35
	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	7.85
1966-75	2.00	0.	0.	0.	0.	0.	0.	0.	0.	0.
1956-75	1.00	0.	0.50	0.	U.	0.	0.	0.	0.	0.
1946-75	0.67	0.33	0.67	0.	0.	0.	0.	0.	0.	0.
1936-75	1.00	1.75	1.00	0.	0.50	0.	0.	0.	0.	0.
1926-75	1.00	3.60	1.20	U.	0.80	0.	0.	0.	0.	0.
1916-75	0.83	3.17	1.17	0.	0.67	0.	0.	0.	0.	0.
1906-75	0.71	2.86	1.00	0.	0.57	0.	0.	0.	0.	0.
1896-75	0.63	2.50	1.00	0.	0.50	0.	0.	0.	0.	0.
1886-75	0.56	2.44	0.89	0.	0.44	0.	0.	0.	U.	0.
1876-75	0.60	2.30	0.90	0.10	0.40	0.	0.	0.	0.	0.
1866-75	0.55	2.18	0.91	0.09	0.45	0.	0.	0.	0.	0.
1856-75	0.50	2.00	0.63	0.08	U.42	0.	0.	0.	0.	0.
1846-75	0.46	1.85	0.77	0.08	0.38	0.	0.	0.	0.	0.
1836-75	0.50	1.71	0.71	0.07	0.36	0.	0.	0.	0.	0.
1826-75	0.47	1.60	0.67	0.07	0.33	0.	0.	0.	0.	0.
1816-75	0.44	1.50	0.63	U.06	0.31	0.	0.	0.	0.	0.
1806-75	0.41	1.41	0.59	0.06	0.29	0.	0.	0.	0.	0.

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Table 12

TEN YEAR ACTIVITY RATES

SOURCE REGION NORTHERN ILLINOIS AREA * 55128 KM++2

				me-							
YR/MB	2.85	3.35	3,85	4,35	4.85	5.35	5.85 6.35	6.35	6.85	7.35	SUM
1966-75	0	0	0	1	0	0	0	0	0	0	1
1956-65	U	Ú	0		0	0	0	0	0	0	0
1946-55	C	1	U	0	0	0	0	0	0	0	1
1936-45	4	1	1		0	0	0	0	0	0	6
1926-35	0	2	2	1	0	0	0	0	0	0	5
1916-25	C	0	0	0	0	0	0	0	0	0	0
1906-15	0	4	1	1	1	0	0	0	0	0	7
1896 -5	0	0	U	0	0	0	0	0	0	0	0
1886-95	6	0	U	0	0	0	0	0	0	0	0
1876-85	C	0	U	1	0	0	0	0	0	0	1
1866-75	U	0	U	0	0	0	0	0	0	0	0
1856-65	0	0	U	0	0	0	0	0	0	0	0
1846-55	0	0	U	0	0	0	0	0	0	0	0
1836-45	0	0	U		0	0	0	0	0	0	0
1826-35	U	0	U	•	0	0	0	0	0	0	0
1816-25	0	0	0		0	0	0	0	0	0	0
1806-15	Q	0	0	•	0	0	0	0	0	0	0
SUM MAG	4	8	4	4	1	0	0	0	0	0	21

YR/MB	2.85	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35
	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	7.85
1966-75	0.	0.	0.	1.00	0.	0.	0.	0.	0.	0.
1956-75	0.	0.	0.	0.50	0.	0.	0.	0.	0.	0.
1946-75	0.	0.33	U.	0.33	0.	0.	0.	0.	0.	0.
1936-75	1.00	0.50	0.25	0.25	0.	0.	0.	0.	0.	0.
1926-75	0.80	0.80	0.00	0.40	0.	0.	0.	0.	0.	0.
916-75	0.67	0.67	0.50	0.33	0.	0.	0.	0.	0.	0.
906-75	0.57	1.14	4.57	0.43	0.14	0.	0.	0.	0.	0.
896-75	0.50	1.00	0.50	0.38	0.13	0.	0.	0.	0.	0.
886-75	U. 44	0.89	U. 44	0.33	0.11	0.	0.	0.	0.	0.
876-75	0.40	0.60	0.40	0.40	0.10	0.	0.	0.	0.	0.
866-75	0.36	0.73	0.36	0.36	0.09	0.	0.	0.	0.	0.
856-75	0.33	0.67	0.33	0.33	0.08	0.	0.	0.	0.	0.
846-75	0.31	0.62	0.31	0.31	0.08	0.	0.	0.	0.	0.
836-75	0.29	0.57	0.29	0.29	0.07	0.	0.	0.	0.	0.
826-75	0.27	0.53	0.27	0.27	0.07	0.	0.	0.	O.	0.
816-75	0.25	0.50	0.25	0.25	0.06	0.	0.	0.	0.	0.
806-75	0.24	0.47	0.24	0.24	0.06	0.	0.	0.	0.	0.

Table 13

TEN YEAR ACTIVITY RATES

SOURCE REGION NEMAHA RIDGE AREA = 206071 KM++2

YR/MB	2.85	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	SUM
	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	7.85	DECAD
1966-75	2	1	0	G	0	0	0	0	0	0	3
1956-65	1	0	Ü	1	0	0	0	0	0	0	2
1946-55	2	6	2	8	0	1	0	0	0	0	14
1936-45	U	2	1	0	0	0	0	0	0	0	3
1926-35	2	1	5	2	1	0	0	0	0	0	11
1916-25	1	4	1	2	0	0	0	0	0	0	8
1906-15	0	2	U		0	0	0	0	0	0	2
1896 -5	5	4	U		0	1	0	0	0	0	10
1886-95	0	0	Ü		0	0	0	0	0	0	0
1876-85	C	n	U	0	1	0	0	0	0	0	1
1866-75	0	2	1		1	0	0	0	0	0	4
1856-65	U	0	ū		0	0	0	0	0	0	0
1846-55	0	0	L.	n	0	0	0	0	0	0	n
1836-45	U	0	ü	0	0	0	0	0	0	Ō	0
1826-35	C	0	0	A	0	0	0	0	0	0	0
1816-25	0	D	Ü	ä	Ö	ō	Ō	ō	0	ō	n
1806-15	· ·	Ü	Ü	9	Ö	Ō	0	ō	0	Ō	Ö
SUM MAG	13	22	10		3	2	0	0	0	0	58

						The state of the s	Carried William Carried			
YR/MB	2.85	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35
	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	7.85
1966-75	2.00	1.00	0.	0.	0.	0.	0.	0.	0.	0.
1956-75	1.50	0.50	0.	0.90	0.	0.	0.	0.	0.	0.
1946-75	1.67	2.33	0.67	1.33	U.	0.33	0.	0.	0.	0.
1936-75	1.25	2.25	0.75	1.00	0.	0.25	0.	0.	0.	0.
1926-75	1.40	2.00	1.60	1.20	0.20	0.20	0.	0.	0.	0.
1916-75	1.33	2.33	1.50	1.33	0.17	0.17	0.	0.	0.	0.
1906-75	1.14	2.29	1.29	1.14	0.14	0.14	0.	0.	0.	0.
1896-75	1.63	2.50	1.13	1.00	0.13	0.25	0.	0.	0.	0.
1886-75	1.44	2.22	1.00	0.89	0.11	0.22	0.	0.	0.	0.
1876-75	1.30	2.00	0.90	0.80	0.20	0.20	0.	0.	0.	0.
1866-75	1.18	2.00	0.91	0.73	0.27	0.18	0.	0.	0.	0.
1856-75	1.08	1.83	0.83	0.67	0.25	0.17	0.	0.	0.	0.
1846-75	1.00	1.69	0.77	0.62	0.23	0.15	0.	0.	0.	0.
1836-75	0.93	1.57	0.71	0.57	0.21	0.14	0.	0.	0.	0.
1826-75	0.87	1.47	0.67	0.93	0.20	0.13	0.	0.	0.	0.
1816-75	0.81	1.38	0.63	0.90	0.19	0.13	0.	0.	0.	0.
1806-75	0.76	1.29	0.59	0.47	0.18	0.12	0.	0.	0.	0.

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Table 14

TEN YEAR ACTIVITY RATES

SCURCE REGION NORTHERN GREAT PLAINS AREA = 426723 KM++2

YR/MB	2.85	3.35	3.85	4,35	4.85	5.35	5,85	6.35	6.85	7.35	SUM
	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	7.85	DECADE
1966-75	1	3	U	2	0	0	0	0	0	0	6
1956-65	1	6	1	2	0	0	0	0	0	0	10
1946-55	1	11	U		0	0	0	0	0	0	12
1936-45	0	6	4	1	0	0	0	0	0	0	11
1926-35	1	7	4	1	0	0	0	0	0	0	13
1916-25	0	6	U	f	0	0	0	٥	0	٥	7
1906-15	1	3	3	1	0	0	0	0	0	0	8
1896 -5	0	5	U	2	0	0	0	0	0	0	5
1886-95	U	1	2	0	0	0	0	0	0	0	3
1876-85	U	1	1	0	1	0	0	0	0	0	3
1866-75	0	2	1	6	ō	0	0	0	0	0	3
1856-65	0	0	0	0	0	0	0	0	0	0	0
1846-55	0	0	0		0	0	0	0	0	0	0
1836-45	0	0	U	0	Ö	0	0	0	0	0	0
1826-35	0	0	U	0	0	0	0	0	0	0	0
1816-25	0	0	U	G	Ö	0	0	0	0	0	0
1806-15	U	n	U	0	0	0	0	0	0	0	0
SUM MAG	5	49	16	10	1	0	0	0	0	0	81

YR/MB	2.85	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35
1966-75										0.
	1.00	3.00	0.	2.00	0.	0.	0.	0.	0.	
1956-75	1.00	4.50	0.50	2.00	U.	0.	0.	0.	0.	0.
1946-75	1.00	6.67	0.33	1.33	0.	θ.	0.	0.	0.	0.
1936-75	0.75	6.50	1.25	1.25	U.	0.	0.	0.	0.	0.
1926-75	0.80	6.60	1.00	1.20	0.	0.	0.	0.	0.	0.
1916-75	0.67	6.50	1.50	1.17	0.	0.	0.	0.	0.	0.
1906-75	0.71	6.00	1./1	1.14	0.	0.	0.	0.	0.	0.
1896-75	0.63	5.63	1.50	1.25	U .	0.	0.	0.	0.	0.
1886-75	0.56	5.11	1.56	1.11	0.	0.	0.	0.	0.	0.
1876-75	0.50	4.70	1.50	1.00	0.10	0.	0.	0.	0.	0.
1866-75	0.45	4.45	1.45	0.91	0.09	0.	0.	0.	0.	0.
1856-75	0.42	4.08	1.33	0.83	0.08	0.	0.	0.	0.	0.
1846-75	0.38	3.77	1.23	0.77	0.08	0.	0.	0.	0.	0.
1836-75	0.36	3.50	1.14	0.71	0.07	0.	0.	0.	0.	0.
1826-75	0.33	3.27	1.07	0.67	0.07	0.	0.	0.	0.	0.
1816-75	0.31	3.06	1.00	0.63	U.06	0.	0.	0.	0.	0.
1806-75	0.29	2.88	U.94	0.59	0.06	0.	0.	0.	0.	0.

Table 15

TEN YEAR ACTIVITY RATES

SOURCE REGION WICHITA-OUACHITA AREA * 261829 KM++2

YR/MB	2.85	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	SUM
	3.35	3.85	4.35	4.85	5.35	5.85	6,35	6.85	7.35	7.85	DECADE
1966-75	3	7	3	3	0	0	0	0	0	0	16
1956-65	3	4	4	2	0	0	0	0	0	0	13
1946-55	2	10	3	4	0	1	0	0	0	0	20
1936-45	0	2	3	0	. 0	0	0	0	0	0	5
1926-35	3	1	3	3	0	0	0	0	0	0	10
1916-25	3	1	3	9	0	0	0	0	0	0	12
1906-15	1	5	1	1	U	0	0	0	0	0	5
1896 -5	0	1	U	0	0	0	0	0	0	0	1
1886-95	0	1	U	0	0	0	0	0	0	0	1
1876-65	U	ü	U	0	0	0	0	0	0	0	0
1866-75	0	0	Ü		0	0	0	0	0	0	0
1856-65	U	0	U	0	0	0	0	0	0	0	0
1846-55	C	0	U	0	0	0	0	0	0	0	Ď.
1836-45	0	0	U	0	0	0	0	0	0	0	0
1826-35	0	0	0		0	0	0	0	0	0	0
1816-25	0	0	Ü	0	0	0	0	0	0	0	0
1806-15	0	ū	Ü	8	0	0	0	0	0	0	0
SUM MAG	15	29	20	18	0	1	0	0	0	0	83

YR/MB	2.85	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35
	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	7.85
1966-75	3.00	7.00	3.00	3.00	0.	0.	0.	0.	0.	0.
1956-75	3.00	5.50	3.50	2.50	0.	0.	0.	0.	0.	0.
1946-75	2.67	7.00	3.53	3.00	0.	0.33	0.	0.	0.	0.
1936-75	2.00	5.75	3.45	2.25	0.	0.25	0.	0.	0.	0.
1926-75	2.20	4.80	3.20	2.40	0.	0.20	0.	0.	0.	0.
1916-75	2.33	4.17	3.17	2.83	0.	0.17	0.	0.	0.	0.
1906-75	2.14	3.86	2.86	2.57	0.	0.14	0.	0.	0.	0.
1896-75	1.88	3.50	2.50	2.25	0.	0.13	0.	0.	0.	0.
1886-75	1.67	3.22	2.22	2.00	0.	0.11	0.	0.	0.	0.
1876-75	1.50	2.90	2.00	1.80	0.	0.10	0.	0.	0.	0.
1866-75	1.36	2.64	1.82	1.64	0.	0.09	0.	0.	0.	0.
1856-75	1.25	2.42	1.67	1.90	0.	0.08	0.	0.	0.	0.
1846-75	1.15	2.23	1.54	1.38	0.	0.08	0.	0.	0.	0.
1836-75	1.07	2.07	1.43	1.29	0.	0.07	0.	0.	0.	0.
1826-75	1.00	1.93	1.33	1.20	0.	0.07	0.	0.	0.	0.
1816-75	0.94	1.81	1.25	1.13	0.	0.06	0.	0.	0.	0.
1806-75	0.88	1.71	1.18	1.06	0.	0.06	0.	0.	0.	0.

THIS PAGE IS BEST QUALITY FRACTICABLE FROM COFY FURNISHED TO DDC

Table 16

TEN YEAR ACTIVITY RATES

SCURCE REGION WABASH VALLEY AREA # 39780 KM++2

			-	WE	37/00	744-5					
YR/MB	2.85	3.35	3.85	4.35	4.85	5.35	5,85	6.35	6.85	7.35	SUM
	3.35	3.85	4.35	4.85	5.35	5.85	6,35	6.85	7.35	7.85	DECADE
1966-75	3	1	U	1	0	1	0	0	0	0	6
1956-65	1	1	C	2	0	0	0	0	0	0	4
1946-55	1	2	1	6	0	0	0	0	0	0	4
1936-45	0	2	1	0	0	0	0	0	0	0	3
1926-35	1	3	1	0	0	0	0	0	0	0	5
1916-25	0	4	6	4	2	0	0	0	0	0	16
1906-15	0	4	~	8	1	0	0	ō	0	0	7
1896 -5	Û	3	U	0	1	0	0	0	0	0	4
1886-95	0	n	0	,	0	0	0	Ö	0	0	2
1876-85	0	2	0	0	0	0	0	0	0	0	2
1866-75	0	2	0	2	0	0	0	ō	0	Ö	4
1856-65	C	0	U	1	0	0	0	0	0	0	-
1846-55	0	0	Ü	8	0	0	0	0	0	Ö	ō
1836-45	0	0	u	0	0	0	0	0	0	0	0
1826-35	U	0	0		0	0	0	0	0	0	0
1816-25	0	0	U		0	0	0	Ô	Ō	0	n
1806-15	Ü	0	U	0	Ö	0	0	ō	0	0	Ö
SUM MAG	6	24	11	12	4	1	0	0	0	0	58

YR/MB	2.05	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35
	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	7.85
1966-75	3.00	1.00	0.	1.00	0.	1.00	0.	0.	0.	0.
1956-75	2.00	1.00	0.	1.50	0.	0.50	0.	0.	0.	0.
1946-75	1.67	1.33	0.33	1.00	0.	0.33	0.	0.	0.	0.
1936-75	1.25	1.50	0.50	0.75	0,	0.25	0.	0.	0.	0.
1926-75	1.20	1.80	0.60	0.60	0.	0.20	0.	0.	0.	0.
916-75	1.00	2.17	1.50	1.17	0.33	0.17	0.	0.	0.	0.
906-75	0.86	2.43	1.57	1.00	0.43	0.14	0.	0.	0.	0.
896-75	0.75	2.50	1.38	0.88	0.50	0.13	0.	0.	0.	0.
1886-75	0.67	2.22	1.22	1.00	0.44	0.11	0.	0:	0.	
876-75	0.60	2.20	1.10	0.90	0.40	0.10	0.	0.	0.	0.
1866-75	0.55	2.18	1.00	1.00	0.36	8.09	0.	0.	U .	0.
1856-75	0.50	2.00	0.92	1.00	0.33	0.08	0.	0.	U.	0.
846-75	0.46	1.85	0.85	0.92	0.31	0.08	0.	0.	0.	0.
836-75	0.43	1.71	0.19	0.86	0.29	0.07	0.	0.	0.	0.
826-75	0.40	1.60	0.73	0.60	0.27	0.07	0.	0.	0.	0.
816-75	0.38	1.50	0.69	0.75	0.25	0.06	0.	0.	0.	0.
1806-75	0.35	1.41	0.65	0.71	0.24	0.06	0.	0.	0.	0.

TEN YEAR ACTIVITY RATES

SOURCE REGION OZARK UPLIFT AREA # 36557 KM++2

YR/MB	2.85	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	SUM
	• • •	• • • •	,,,,,								
1966-75	4	3	2		0	0	0	0	0	0	9
1956-05	4	4	0	0	1	0	0	0	0	0	9
1946-55	0	2	2	3	0	0	0	0	0	0	7
1936-45	1	5	1	3	1	0	0	0	0	0	11
1926-35	5	12	1		0	0	0	0	0	0	15
1916-25	2	5	9	0	1	0	0	0	0	0	17
1906-15	0	2	2		0	0	0	0	0	0	4
1896 -5		1	0	2	0	0	0	0	0	0	4
1886-95	3	3	0		0	0	0	0	0	0	3
1876-85	0	2	4	1	U	0	0	0	0	0	7
1866-75	0	2	U	9	0	0	0	0	0	0	2
1856-65	0	0	U	0	1	0	0	0	0	0	ī
1846-55	0	0	U	0	0	0	0	0	0	0	0
1836-45	0	0	U		0	1	0	0	0	0	1
1826-35	0	U	U	6	0	0	0	0	0	0	0
1816-25	0	2	1		0	0	0	0	0	0	3
1806-15	Q	0	Ú		0	0	0	0	0	0	0
SUM MAG	14	43	22	9	4	1	0	0	0	0	93

2.65	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35
3.35	3.85	4.35	4.65	5.35	5.85	6.35	6,85	7.35	7.85
4.00	3.00	2.00	0.	0.	0.	0.	0.	0.	0.
4.00	3.50	1.00	0.	0.50	0.	0.	0.	0.	0.
2.67	3.00	1.33	1.00	0.33	0.	0.	0.	0.	0.
2.25	3.50	1.25	1.90	0.50	0.	0.	0.	0.	0.
2.20				0.40	0.			0.	0.
2.17				0.50	0.		0.	0.	0.
1.86	4.71	2.43	0.86	0.43	0.		0.	0.	0.
1.75	4.25	2.13	1.00	0.38	0.		0.	0.	0.
1.56		1.69	0.89	0.33	0.			0.	0.
1.40	3.90	2.10	0.90	0.30	0.	0.	0.	0.	0.
1.27	3.73	1.91	0.82	0.27	0.	0.	0.	0.	0.
1.17	3.42	1.75	0.75	0.33	0.	0.	0.	0.	0.
1.08	3,15	1.62	0.69	0.31	0.	0.	0.	0.	0.
1.00	2.93	1.50	0.64	0.29	0.07	0.	0.	0.	0.
0.93	2.73	1.40	0.60	0.27	0.07	0.	0.	0.	0.
0.68	2.69	1.38	0.56	0.25	0.06	0.	0.	0.	0.
0.82	2.53	1.29	0.53	0.24	0.06	0.	0.	0.	0.
	3.35 4.00 4.00 2.67 2.25 2.20 2.17 1.86 1.75 1.40 1.27 1.17 1.08 1.09 0.68	3.35 3.85 4.00 3.00 4.00 3.50 2.67 3.00 2.25 3.50 2.20 5.20 2.17 5.17 1.86 4.71 1.75 4.25 1.56 4.11 1.40 3.15 1.08 3.15 1.08 3.15 1.08 2.93 0.93 2.93 0.68 2.69	3.35 3.85 4.35 4.00 3.00 2.00 4.00 3.50 1.00 2.67 3.00 1.33 2.25 3.50 1.25 2.20 5.20 1.20 2.17 5.17 2.59 1.86 4.71 2.43 1.75 4.25 2.13 1.56 4.11 1.69 1.40 3.90 2.10 1.27 3.73 1.91 1.17 3.42 1.75 1.08 3.15 1.62 1.08 3.15 1.62 1.09 2.93 1.59 0.93 2.73 1.40 0.68 2.69 1.38	3.35 3.85 4.35 4.65 4.00 3.00 2.00 0. 4.00 3.50 1.00 0. 2.67 3.00 1.33 1.60 2.25 3.50 1.25 1.50 2.20 5.20 1.20 1.20 2.17 5.17 2.50 1.60 1.86 4.71 2.43 0.86 1.75 4.25 2.13 1.00 1.56 4.11 1.69 0.89 1.40 3.90 2.10 0.90 1.27 3.73 1.91 0.82 1.17 3.42 1.75 0.75 1.08 3.15 1.62 0.69 1.00 2.93 1.50 0.64 0.93 2.73 1.40 0.66 0.68 2.69 1.38 0.56	3.35 3.85 4.35 4.65 5.35 4.00 3.00 2.00 0. 0. 4.00 3.50 1.00 0. 0.50 2.67 3.00 1.33 1.60 0.33 2.25 3.50 1.25 1.50 0.50 2.20 5.20 1.20 1.20 0.40 2.17 5.17 2.50 1.60 0.50 1.86 4.71 2.43 0.86 0.43 1.75 4.25 2.13 1.00 0.38 1.56 4.11 1.69 0.89 0.33 1.40 3.90 2.10 0.90 0.30 1.27 3.73 1.91 0.82 0.27 1.17 3.42 1.75 0.75 0.33 1.08 3.15 1.62 0.69 0.31 1.08 3.15 1.62 0.69 0.31 1.08 3.15 1.62 0.69 0.31 1.09 2.93 1.50 0.64 0.29 0.93 2.73 1.40 0.60 0.27 0.68 2.69 1.38 0.56 0.25	3.35 3.85 4.35 4.65 5.35 5.85 4.00 3.00 2.00 0. 0. 0. 0. 4.00 3.50 1.00 0. 0.50 0. 2.67 3.00 1.33 1.00 0.33 0. 2.25 3.50 1.25 1.90 0.50 0. 2.20 5.20 1.20 1.20 0.40 0. 2.17 5.17 2.50 1.60 0.50 0. 1.86 4.71 2.43 0.86 0.43 0. 1.75 4.25 2.13 1.00 0.38 0. 1.56 4.11 1.69 0.89 0.33 0. 1.40 3.90 2.10 0.90 0.30 0. 1.27 3.73 1.91 0.82 0.27 0. 1.17 3.42 1.75 0.75 0.33 0. 1.08 3.15 1.62 0.69 0.31 0. 1.08 3.15 1.62 0.69 0.31 0. 1.09 2.93 1.50 0.64 0.29 0.07 0.93 2.73 1.40 0.60 0.27 0.07 0.68 2.69 1.38 0.56 0.25 0.06	3.35 3.85 4.35 4.85 5.35 5.85 6.35 4.00 3.00 2.00 0. 0. 0. 0. 0. 4.00 3.50 1.00 0. 0.50 0. 0. 2.67 3.00 1.33 1.80 0.33 0. 0. 2.25 3.50 1.25 1.50 0.50 0. 0. 2.20 5.20 1.20 1.20 0.40 0. 0. 2.17 5.17 2.50 1.60 0.50 0. 0. 1.86 4.71 2.43 0.86 0.43 0. 0. 1.75 4.25 2.13 1.00 0.38 0. 0. 1.75 4.25 2.13 1.00 0.38 0. 0. 1.56 4.11 1.69 0.89 0.33 0. 0. 1.40 3.90 2.10 0.90 0.30 0. 0. 1.27 3.73 1.91 0.82 0.27 0. 0. 1.17 3.42 1.75 0.75 0.33 0. 0. 1.08 3.15 1.62 0.69 0.31 0. 0. 1.08 3.15 1.62 0.69 0.31 0. 0. 1.09 2.93 1.50 0.64 0.29 0.07 0. 0.93 2.73 1.40 0.60 0.27 0.07 0. 0.68 2.69 1.38 0.56 0.25 0.06 0.	3.35 3.85 4.35 4.65 5.35 5.85 6.35 6.85 4.00 3.00 2.00 0. 0. 0. 0. 0. 0. 0. 4.00 3.50 1.00 0. 0.50 0. 0. 0. 0. 2.67 3.00 1.33 1.00 0.33 0. 0. 0. 0. 2.25 3.50 1.25 1.50 0.50 0. 0. 0. 2.20 5.20 1.20 1.20 0.40 0. 0. 0. 2.17 5.17 2.50 1.00 0.50 0. 0. 0. 0. 2.17 5.17 2.50 1.00 0.50 0. 0. 0. 0. 1.86 4.71 2.43 0.86 0.43 0. 0. 0. 0. 1.75 4.25 2.13 1.00 0.38 0. 0. 0. 0. 1.56 4.11 1.69 0.89 0.33 0. 0. 0. 0. 1.40 3.90 2.10 0.90 0.30 0. 0. 0. 1.27 3.73 1.91 0.82 0.27 0. 0. 0. 1.27 3.73 1.91 0.82 0.27 0. 0. 0. 1.17 3.42 1.75 0.75 0.33 0. 0. 0. 0. 1.08 3.15 1.62 0.69 0.31 0. 0. 0. 1.08 3.15 1.62 0.69 0.31 0. 0. 0. 0. 1.00 2.93 1.50 0.64 0.29 0.07 0. 0. 0. 0. 0.93 2.73 1.40 0.60 0.27 0.07 0. 0. 0. 0. 0.68 2.69 1.38 0.56 0.25 0.06 0. 0.	3.35 3.85 4.35 4.65 5.35 5.85 6.35 6.85 7.35 4.00 3.00 2.00 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.

Table 18

TEN YEAR ACTIVITY RATES

SOURCE REGION NEW MADRID A AREA = 22506 KM++2

YR/MB	2.85	3.35	3.85	4.35	4.85	5.35	5,85	6.35	6.85	7.35	SUM
	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	7,85	DECADE
1966-75	15	10	4	1	0	0	0	0	0	0	30
1956-65	11	9	10	6	0	0	0	0	0	0	30
1946-55	8	19	8	9	0	0	0	0	0	0	40
1936-45	5	17	1	2	0	0	0	0	0	0	25
1926-35	6	14	3	1	1	0	0	0	0	0	25
1916-25	0	5	1	1	1	0	0	0	0	0	14
1906-15	Ü	0	3	3	Ō	0	0	Ö	0	0	6
1896 -5	1	2	4	2	2	0	0	0	0	0	11
1886-95	ō	9	6	A	0	Ö	0	Ď.	0	0	9
1876-85	0		5	1	1	0	0	0	0	0	A
1866-75	2	1	2	•	ō	0	0	0	0	0	A
1856-65	. 0	5	0		1	0	0	0	0	0	4
1846-55	0	•	1	· ;	ō	0	0	o	0	0	4
1836-45	0	7	3	•	0	0	1	0	0	0	8
1826-35	0	0	0	•	0	0	ō	0	0	0	Ô
1816-25	0	2	r.		0	0	0	0	0	0	2
1806-15	ō	2	0		0	0	0	0	2	1	5
1000-17	•	-	U	0	·		•	•			,
SUM MAG	48	100	51	20	6	0	1	0	2	1	229

YR/MB	2.65	3.35	3.85	4.35	4.85	5.35	5,85	6.35	6.85	7.35
	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	7.8
1966-75	15.00	10.00	4.00	1.00	0.	0.	0.	0.	0.	0.
1956-75	13.00	9.50	7.00	0.50	0.	0.	0.	0.	0.	0.
1946-75	11.33	12.67	7.33	2.00	0.	0.	0.	0.	0.	0.
1936-75		13.75	5.75	2.00	U.	0.	0.	0.	0.	0.
1926-75	9.00	13.80	5.20	1.80	0.20	0.	0.	0.	0.	0.
1916-75			5.50	1.67	0.33	0.	0.	0.	0.	0.
1906-75		10.57	5.14	1.86	0.29	0.	0.	0.	0.	0.
1896-75		9.50	5.00	1.88	0.50	0.	0.	0:	0.	0.
1886-75		9.44	4.44	1.67	0.44	0.	0.	0.	0.	0.
1876-75		8.60	4.50	1.60	0.50	0.	0.	0.	0.	0.
1866-75		8.18	4.27	1.45	0.45	C.	0.	0.	0.	0.
1856-75	4.00	7.67	3.92	1.42	0.50	0.	0.	0.	0.	0.
1846-75		7.15	3.69	1.46	0.46	0.	0.	0.	0.	0.
1836-75		6.86	3.64	1.43	0.43	0.	0.07	0.	0.	0.
1826-75	3.20	6.40	3.40	1.33	0.40	0.	0.07	0.	0.	0.
1816-75	3.00	6.13	3.19	1.25	0.38	0.	0.06	0.	0.	0.
1806-75	2.82	5.88	3.00	1.18	0.35	0.	0.06	0.	0.12	0.06

TEN YEAR ACTIVITY RATES

SCURCE REGION NEW MADRID B

YR/MB	2.85	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	SUM
	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	7.85	DECADE
1966-75	1	0	0	6	0	0	0	o	0	0	1
1956-65	3	4	1	2	0	0	0	U	0	0	10
1946-55	1	2	0	1	0	0	0	0	0	0	4
1936-45	1	3	1	Í	0	0	0	0	0	0	6
1926-35	2	5	1	1	0	0	0	0	0	0	9
1916-25	0	6	2	1	0	0	0	0	0	0	9
1906-15	0	3	3	1	0	0	0	0	0	0	7
1896 -5	U	0	1	1	0	0	0	0	0	0	2
1886-95	O	4	1	1	0	0	1	0	0	0	7
1876-85	O	3	3	- Ž	0	Ö	ō	ō	O	0	8
1866-75	0	1	u	0	0	0	0	0	0	0	3
1856-65	0	0	. 0		Ō	0	0	G	.0	0	0
1846-55	U	2	0	0	0	0	0	0	0	0	2
1836-45	0	•	ú		0	0	0	0	0	0	1
1826-35	0	n	Ü		ō	ō	0	0	0	0	Ô
1816-25	0	0	1		0	0	0	0	0	0	1
1806-15	C	Ö	ō		Ö	Ō	0	ō	0	ō	0
SUM MAG	8	36	14	11	0	0	1	0	C	0	70

CUMULATIVE ACTIVITY RATES PER DECADE

YR/MB	2.65	3.35	3.85	4.85	4.85	5.35	5.85	6.35	6.85	7.35
	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35	7.85
1966-75	1.00	0.	0.	0.	0.	0.	0.	0.	0.	0.
1956-75	2.00	2.00	0.50	1.00	0.	0.	0.	0.	0.	0.
1946-75	1.67	2.00	0.33	1.00	U.	0.	0.	0.	0.	0.
1936-75	1.50	2.25	0.50	1.00	0.	0.	0.	0.	0.	0.
1926-75	1.00	2.80	0.60	1.00	U.	0.	0.	0.	0.	0.
1916-75	1.33	3.33	0.83	1.00	0.	0.	0.	0.	0.	0.
1906-75	1.14	3,29	1.14	1.00	U.	0.	0.	0.	0.	0.
1896-75	1.00	2.88	1.13	1.00	0.	0.	0.	0.	0.	0.
1886-75	0.89	3.00	1.11	1.00	0.	0.	0.11	0.	0.	0.
1876-75	0.80	3.00	1.30	1.10	0.	0.	0.10	0.	0.	0.
1866-75	0.73	3.00	1.18	1.00	0.	0.	0.09	0.	0.	0.
1856-75	0.67	2.75	1.08	0.92	0.	0.	0.08	0.	0.	0.
1846-75	0.62	2.69	1.00	0.85	0.	0.	0.08	0.	0.	0.
1836-75	0.57	2.57	0.93	0.79	0.	0.	0.07	0.	0.	0.
1826-75	0.53	2.40	0.87	0.73	0.	0.	0.07	0.	0.	0.
1816-75	0.50	2.25	U.88	0.69	0.	0.	0.06	0.	0.	0.
1806-75	0.47	2.12	0.82	0.65	Q.	0.	0.06	0.	0.	0.

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Table 20

TEN YEAR ACTIVITY RATES

SOURCE REGION RESIDUAL EVENTS AREA =6185019 KM++2

				WEN -	10201,	1,					
YR/MB	2.85	3.35	3.85	4,35	4.85	5.35	5.85	6.35	6.85	7.35 7.85	SUM
	3.32	3.05	4.00	4.03	3.03	3.03	0.02	0.03		,,,,,	
1966-75	15	13	3	3	0	0	0	0	0	0	34
1956-65	25	16	13	1	0	0	0	0	0	0	55
1946-55	3	29	8	7	0	0	0	0	0	0	47
1936-45	21	26	2	1	0	0	0	0	0	0	50
1926-35	13	24	16	2	1	1	0	0	0	0	57
1916-25	8	16	12	2	0	0	0	0	0	0	38
1906-15	4	11	3		2	0	0	0	0	0	20
1896 -5	9	23	9	2	1	0	0	0	0	0	44
1886-95	U	2	1		0	0	0	0	0	0	3
1876-85	2	16	2	1	0	1	0	0	0	0	24
1866-75	2	5	2	0	υ	0	0	0	0	0	9
1856-65	0	1	1		1	C	0	0	0	0	3
1846-55	C	4	2	0	0	0	0	0	0	0	6
1836-45	1	n	1	1	0	0	0	0	0	0	3
1876-35	1	2	Ü	4	0	0	0	0	0	0	7
1816-25	0	2	U	0	0	0	0	0	0	0	2
1806-15	0	ō	U	•	Ō	0	0	Ō	0	0	0
SUM MAG	104	192	75	24	5	2	0	0	0	0	402

CUMULATIVE ACTIVITY RATES PER DECADE

YR/MB	2.65	3.35	3.85	4.35	4.85	5.35	5.85	6.35	6.85	7.35
	3.35	3.85	4.35	4.85	5.35	5.85	6,35	6.85	7.35	7.85
1966-75	15.00	13.00	3.00	3.00	0.	0.	0.	0.	0.	0.
1956-75		14.50	8.00	2.00	U.	0.	0.	0.	0.	0.
1946-75	14.33	19.33	8.00	3.67	0.	0.	0.	0.	0.	0.
1936-75	16.00	21.00	6.50	3.00	0.	0.	0.	0.	0.	0.
1926-75	15.40	21.60	8.40	2.80	0.20	0.20	0.	0.	0.	0.
1916-75	14.17	20.67	9.00	2.67	0.17	0.17	0.	0.	0.	0.
1906-75	12.71	19.29	8.14	2.29	0.43	0.14	0.	0.	0.	0.
1896-75	12.25	19.75	8.25	2.25	0.50	0.13	0.	0.	0.	0.
1886-75		17.78	7.44	2.00	0.44	0.11	0.	0.	0.	0.
1876-75		17.80	6.90	1.90	0.40	9.20	0.	0.	0.	0.
1866-75		16.64	6.45	1.73	0.36	0.18	0.	0.	0.	0.
1856-75			6.00	1.58	0.42	0.17	0.	0.	0.	0.
1846-75	The Control of		5.69	1.46	0.38	0.15	0.	0.	0.	0.
1836-75		13.43	5.36	1.43	0.36	0.14	0.	0.	0.	0.
1826-75		12.67	5.00	1.60	0.33	0.13	0.	0.	0.	0.
1816-75		12.00	4.69	1.90	0.31	0.13	0.	0.	0.	0.
1806-75		11.29	4.41	1.41	0.29	0.12	0.	0.	0.	0.

regions. These tables are derived directly from the data given in Tables 1 through 10. In using the data of Tables 11 through 20 to determine the magnitude-recurrence curve, one must examine the data for completeness. For example, consider Table 17 for the Ozark Uplift. All earthquakes of mb greater than 5 are assumed to have been reported for the entire interval 1806 through 1975. Therefore, the columns for which $m_b = 5.35-5.85$ and 4.85-5.35 are complete. For $m_b = 4.35-4.85$ the number of earthquakes per decade is more or less constant back to 1876. Thus the number of earthquakes of that size in a ten-year interval is taken to be 0.90. For $m_b = 3.85-4.35$ the data are taken to be complete back to 1876, indicating 2.0 earthquakes of that magnitude in a ten-year interval. For $m_b = 3.35-3.85$ the data are taken to be complete back to 1886, with 4.0 earthquakes per ten-year interval. The magnitude range 2.85-3.35 is taken to be incomplete even to the present. Data for it are not used for the Ozark Uplift or any other source region.

53. Figures 6 through 15 present the magnitude-recurrence data for the ten seismic source regions of the central United States. The data are taken from Tables 11 to 20, after equalizing to 100,000 km² and compensating for incompleteness in the data for magnitude less than 5. The curves are straight-line fits to the data, assuming a slope of 0.92 and assigning one-half weight to the largest magnitude data point. Table 21 presents the <u>a</u> and m_{b,max} values, as well as the areas of the seismic source regions.

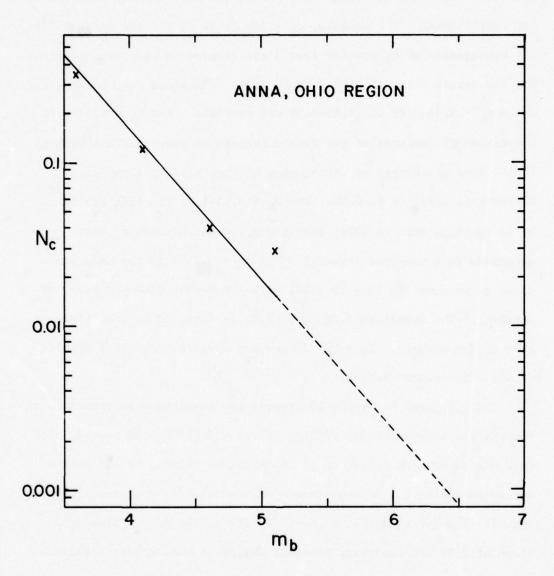


Figure 6. Cumulative magnitude-recurrence curve for the Anna, Ohio region

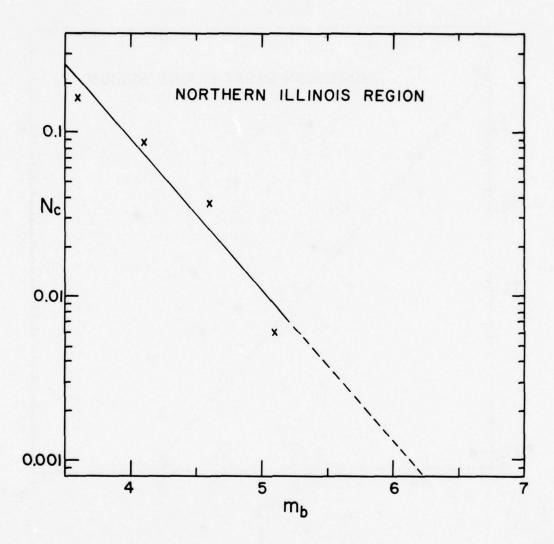


Figure 7. Cumulative magnitude-recurrence curve for the Northern Illinois region

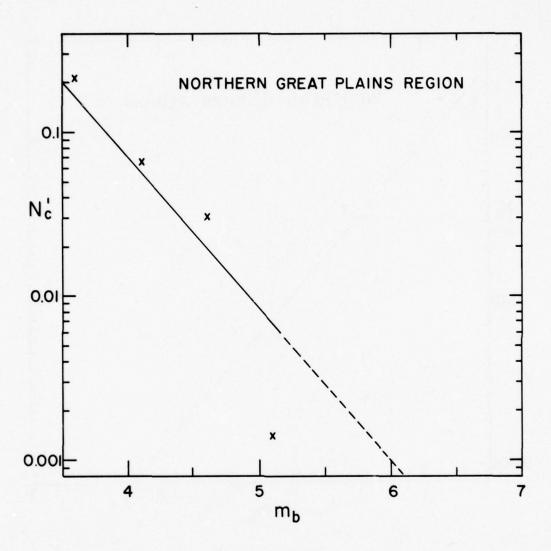


Figure 8. Cumulative magnitude-recurrence curve for the Northern Great Plains region

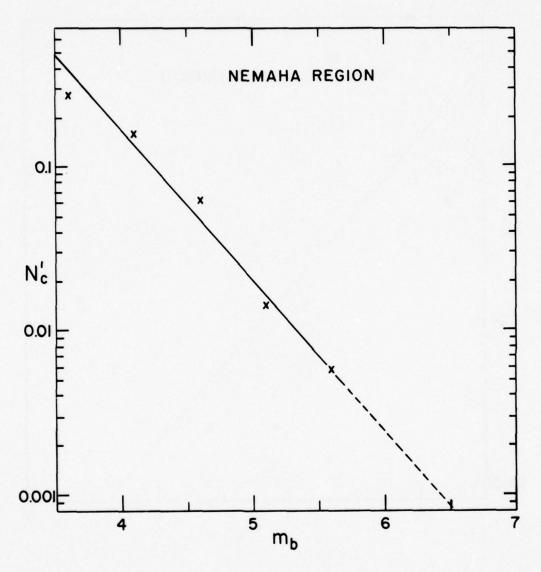


Figure 9. Cumulative magnitude-recurrence curve for the Nemaha region

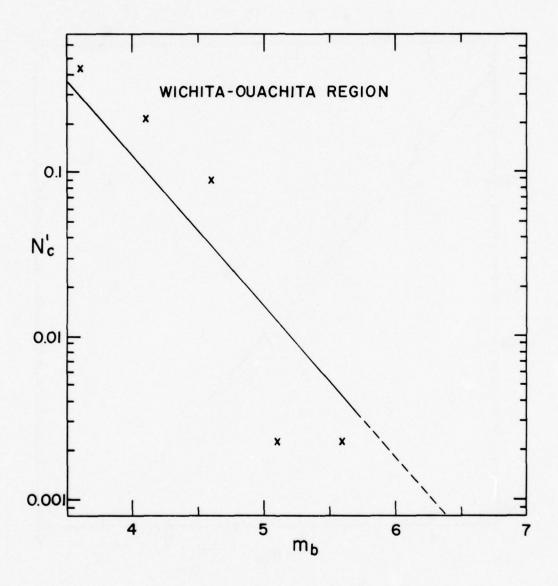


Figure 10. Cumulative magnitude-recurrence curve for the Wichita-Ouachita region

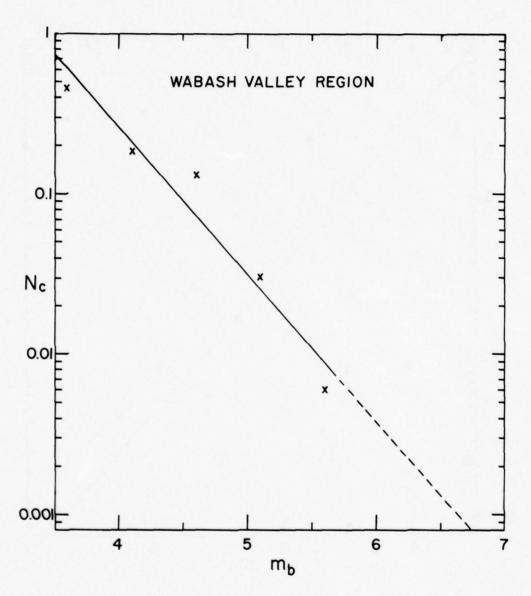


Figure 11. Cumulative magnitude-recurrence curve for the Wabash Valley region

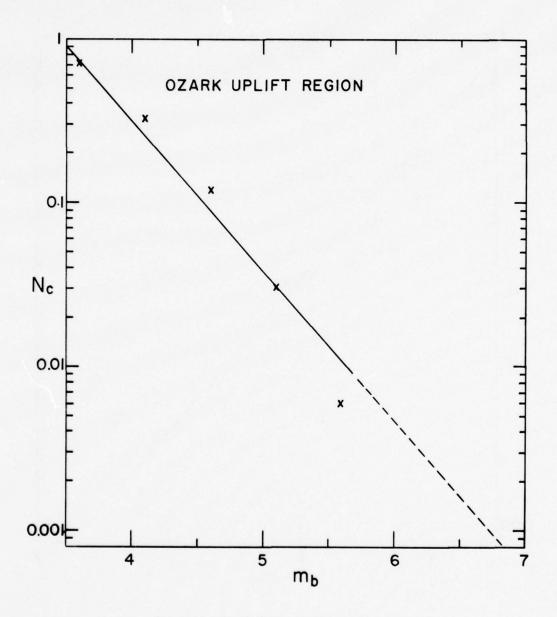


Figure 12. Cumulative magnitude-recurrence curve for the Ozark Uplift region

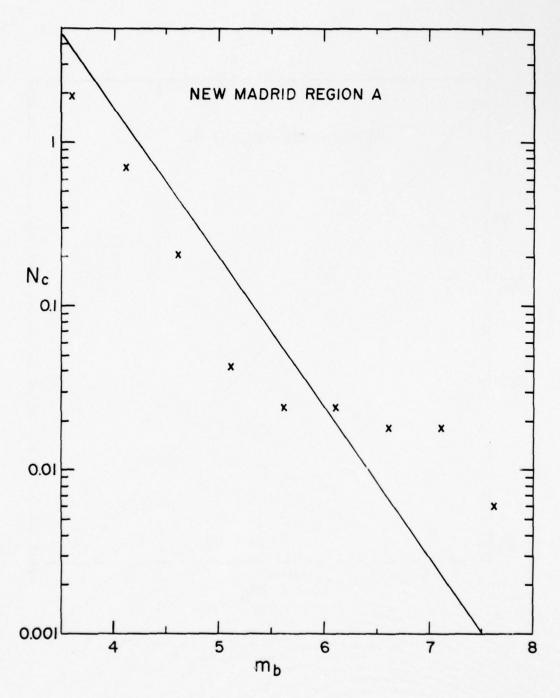


Figure 13. Cumulative magnitude-recurrent New Madrid region

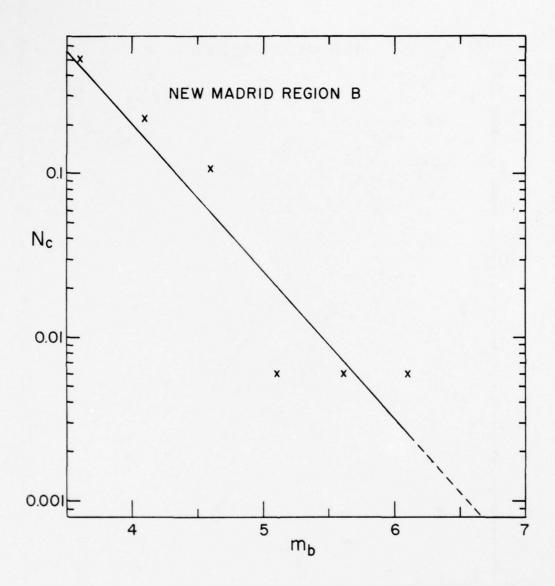


Figure 14. Cumulative magnitude-recurrence curve for New Madrid region B

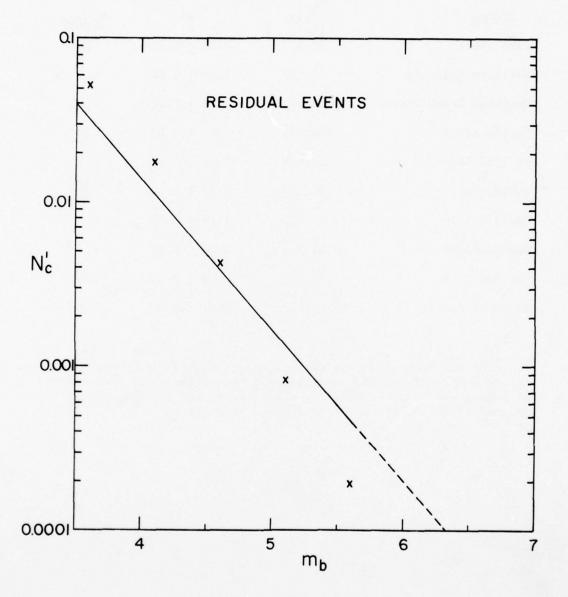


Figure 15. Cumulative magnitude-recurrence curve for the residual events

Table 21
Parameters of Seismic Source Regions

Region	Area (km²)	<u>a</u> 1	m _{b,max}
Anna, Ohio	37,605	2.82 ± 0.12	6.4
Northern Illinois	55,128	2.64 <u>+</u> 0.14	6.1
Northern Great Plains	426,723	2.53 ± 0.31	6.0
Nemaha Ridge	206,071	2.91 <u>+</u> 0.12	6.4
Wichita-Ouachita	261,829	2.79 <u>+</u> 0.47	6.3
Wabash Valley	39,780	3.10 ± 0.16	6.6
Ozark Uplift	36,557	3.19 ± 0.12	6.7
New Madrid A	22,506	3.90 ± 0.53	7.5
New Madrid B	27,506	2.99 <u>+</u> 0.30	6.5
Residual Events	6,185,019	1.83 <u>+</u> 0.21	5.3

 $^{^{1}}$ For the Northern Great Plains, Nemaha Ridge, Wichita-Ouachita and Residual events, the coefficient \underline{a} is indicative of the number of events per 100,000 km 2 . For the other source regions, \underline{a} is indicative of the number of events in the region.

Discussion of Maximum-Magnitude Earthquakes

- 54. Table 21 shows that the New Madrid A seismic source zone is the most active, with a maximum-magnitude earthquake of 7.5. This is the upper limit of the body-wave magnitude scale. That is, no earthquake occurring anywhere in the world will have an m greater than 7.5. The New Madrid B region is found to have an mb.max of 6.5, reflecting the lower level of seismicity in that region for the past 170 years. If one argues on a geological basis that there is no reason to suspect that a large earthquake cannot occur at the ends of the New Madrid fault zone, then regions A and B should be combined into a single source region. This gives an mb.max of 7.5, but with a recurrence period of 800 years instead of 1400 years. Russ²², from a study of fault displacement of recent sediments in western Tennessee near Reelfoot Lake, concludes that the recurrence period for major earthquakes in the New Madrid region is about 666 years. Thus geologic data obtained from trenching of recent sediments are in fairly good agreement with the seismicity data.
- 55. The Ozark Uplift seismic source region consists of a portion of the Illinois basin and the St. Francois highlands of southeast Missouri. The seismicity data do not indicate any separation into two distinct source regions. If such, however, happened to be the case, the maximum-magnitude earthquake for each of the two regions would be about 6.4. Because there is as yet no compelling seismological or

geological reason to separate them into two distinct zones, the more conservative approach of combining them into a single zone with $m_{b,\max}$ of 6.7 is adopted here.

56. For the remainder of the seismic source zones the approximate boundaries appear fairly well established, although they may be subject to variation as more earthquake data become available in the future.

The maximum-magnitude estimates, however, as given in Table 21 are likely to remain unchanged.

PART V: SPECIFICATION OF BEDROCK MOTION

States is very difficult due to the lack of an adequate strong-motion data base upon which to develop empirical correlations between strong ground-motion parameters and some measure of earthquake size, such as maximum Modified Mercalli intensity, $I_{\rm O}$, or body-wave magnitude, $m_{\rm b}$. Reports by Krinitzsky 23 and Krinitzsky and Chang 24 discuss the current strong-motion data base in the western United States, present some correlations and also contain references to other works. The problem of the validity of estimating strong ground motion in the central United States on the basis of the western United States data base still exists.

Maximum Acceleration

- 58. As an attempt at estimating strong ground-motion acceleration in the central United States, some recent empirical results by Murphy and O'Brien²⁵ and theoretical work by Herrmann²⁶ will be used to construct a relationship between acceleration, magnitude and distance for the central United States.
- 59. Using a data set of nearly 1500 strong-motion accelerograms, Murphy and O'Brien²⁵ performed a number of correlations between acceleration, site intensity, magnitude and distance. Correlations were made using vertical components of ground motion as well as the two horizontal components of ground motion. Lacking original accelerogram traces, they made no attempt to rotate the horizontal data into radial or tangential components of motion. Each horizontal observation was treated as an individual data point.
- 60. Murphy and O'Brien²⁵ found that the correlation between maximum acceleration and site intensity is distance dependent (as noted by Krinitzsky and Chang²⁴), and that the error distribution about the predicted accelerations is log-normal with one standard deviation corresponding to a factor of 2 to 2.5. On the basis of residual studies, they proposed a relationship between maximum horizontal acceleration, a, site intensity, I_{MM}, magnitude, M, and epicentral distance, R, of the form

$$\log_{10} a = a I_{MM} + b M + c \log_{10} R + d.$$
 (1)

61. Murphy and O'Brien²⁵ found that this relationship reduced the log-normal standard deviation for maximum horizontal accelerations to a factor of 2.0. They also found that the coefficient "d" exhibited a regional dependence. Their particular relationship used in this study is

$$log_{10} a_{H}(cm/sec^{2}) = 0.14 I_{MM} + 0.24 M - 0.68 log_{10} R + K, (2)$$

where K will be adjusted to fit strong-motion data obtained from earthquakes in the New Madrid seismic zone by Herrmann¹⁴.

62. To apply Equation (2) to the central United States, the following relationships are used:

$$I_0 = 2 m_b - 3.5,$$
 (3)

as given by $Nuttli^4$, where I_O is the maximum Modified Mercalli intensity of an earthquake with body-wave magnitude m_b :

$$I_{MM} = \begin{cases} 0.0 + I_o - 0.00 \log_{10} R, & R \le 20 \text{ km} \\ 3.1 + I_o - 2.46 \log_{10} R, & R \ge 20 \text{ km} \end{cases}$$
 (4)

where I_{NM} is the site intensity at a distance R kilometers from a source with maximum intensity I_{o} . This simple relationship approximates the relation given by Gupta and Nuttli²⁷. Combining Equations (3) and (4), one obtains

$$I_{mm} = \begin{cases} -3.5 + 2 m_b - 0.00 \log_{10}R, & R \le 20 \text{ km} \\ -0.4 + 2 m_b - 2.46 \log_{10}R, & R \ge 20 \text{ km} \end{cases}$$
 (5)

Equations (2) and (5) give

$$\log_{10} a_{\rm H} \; ({\rm cm/sec^2}) = \begin{cases} -1.26 + 0.52 \; m_{\rm b} - 0.00 \; \log_{10} \; R + K, \; R \leq 15 \; km \\ -0.06 + 0.52 \; m_{\rm b} - 1.02 \; \log_{10} \; R + K, \; R \geq 15 \; km \end{cases}$$
 (6)

- 63. In the derivation of Equation (6), special consideration was given for R<20 km. This is due to the fact that the Murphy and O'Brien²⁵ correlation had few data points closer than 20 km and because theoretical wave-propagation studies by Herrmann²⁶ indicate that the change in the coefficient of geometrical spreading occurs at a distance of about one source depth, which is at most 15 km for the central United States, as shown by Herrmann¹³. An equivalence of mb and M was assumed since the Murphy and O'Brien²⁵ data set is skewed toward M<6.5, for which the equivalence holds.
- 64. Since Equation (6) depends heavily upon the validity of the Murphy and O'Brien correlation, Equation (6) should not be accepted without some discussion of its applicability. It is almost axiomatic that one can fit any data by multiple regression if one uses enough parameters. The real question at hand is whether the coefficients obtained from the analysis are physically meaningful. The coefficient of geometrical spreading in Equation (6) indicates that the maximum

acceleration attenuates as approximately R⁻¹ at large distances. This is theoretically seen in the work by Herrmann²⁶ for non-attenuating media. Nuttli and Dwyer¹⁵ have shown that, for all practical purposes, anelastic attenuation is minimal for frequencies less than 10 Hz for the central United States out to at least 300 km. Thus the geometrical spreading of Equation (6) is both theoretically and empirically acceptable for the region.

65. The numerical value of the coefficient of the magnitude, mb, requires some consideration. First of all, most correlations show a weak dependence of maximum acceleration upon magnitude, with a tendency of higher accelerations for larger earthquakes. Thus the coefficient 0.52 is not unreasonable. Studies based on the theoretical work of Herrmann²⁶ show that constant stress drop earthquakes are approximately characterized by constant acceleration when the peak accelerations of the constant stress drop earthquakes are compared at the same distance. In seismological terms, at distances greater than a few source dimensions from the earthquake, the Fourier amplitude spectrum of the ground displacement is characterized by a flat level from f = 0 Hz to f = fc, the corner frequency. At frequencies greater than f_c , the amplitude spectrum varies as $(f/f_c)^{-\gamma}$, where γ is a positive number. Usually, $\gamma = 2$. Earthquakes with constant stress drop are such that the zero-frequency spectral level, A(f = 0), and the corner frequency vary such that A(f = 0) $f_c^3 = constant$. If γ is

less than 3, there is a relationship between A(f = 0) and magnitude, even though the stress drop is constant.

- 66. In a study of larger earthquakes of eastern North America recorded by seismographs since 1910, Street and Turcotte¹⁹ noted that the stress drops increased by a factor of ten, from 6 bars to 60 bars, over a range of seismic moments (proportional to A(f = 0)) from 1.0 E23 dyne-cm to 1.0 E27 dyne-cm. The corner frequency for the seismic moment M_0 = 1.0 E23 dyne-cm is about 0.6 Hz. It is not difficult to show, given γ = 2 and the fact that m_b measures 1-Hz spectral amplitudes, that an increase in stress drop of a factor of ten is accompanied by a change of two units in m_b . Thus, using some simple arguments of spectral scaling together with inferences from theoretical studies, log a_H is proportional to 0.5 m_b , and the coefficient of m_b in Equation (6) is acceptable on theoretical as well as observational grounds.
- 67. Thus the coefficients in Equation (6) are reasonable for application to the central United States. It remains to evaluate the coefficient K. The central United States strong-motion data base given by Herrmann consists of nine three-component accelerograms from three earthquakes with m_b of 4.2, 4.5 and 5.0. Data were plotted in the manner of Murphy and O'Brien consists and visually fitted to Equation (6). The data from all 18 horizontal traces were used. The value of K = 0.7 provides a suitable fit. Murphy and O'Brien consists of nine three-component accelerograms from three earthquakes with m_b of 4.2, 4.5 and 5.0. Data were plotted in the manner of Murphy and O'Brien consists of nine three-component accelerograms from three earthquakes with m_b of 4.2, 4.5 and 5.0. Data were plotted in the manner of Murphy and O'Brien consists of nine three-component accelerograms from three earthquakes with m_b of 4.2, 4.5 and 5.0. Data were plotted in the manner of Murphy and O'Brien consists of nine three-component accelerograms from three earthquakes with m_b of 4.2, 4.5 and 5.0. Data were plotted in the manner of Murphy and O'Brien consists of nine three-component accelerograms from three earthquakes with m_b of 4.2, 4.5 and 5.0. Data were plotted in the manner of Murphy and O'Brien consists of nine three-component accelerograms from three-component ac

values differ by only 0.1 units indicates that there is some similarity in earthquake processes and indicates that a main difference between the western and central United States strong motion is primarily due to differences in anelastic attenuation.

- 68. Another way of using Equation (6) is to obtain a value of K which describes the maximum vectorial horizontal acceleration. Visually, one obtains K = 0.9. Figure 16 shows the central United States strong-motion data, together with theoretical curves based upon Equation (6), for several magnitudes. Since Equation (4) overestimates intensities for distances greater than 300 km, and due to the distance range of data used in the Murphy and O'Brien²⁵ correlations, the curves are shown as dashed lines beyond 300 km. For magnitudes greater than m_b = 5, accelerations are not specified at shorter distances due to the lack of observations in the central United States, as well as to the neglect of the effect of fault dimensions upon the geometrical spreading factor, which is controlled by focal depth solely for small magnitude earthquakes. Another reason is due to the difficulty of specifying the ground-motion spectrum at short distances.
- 69. The recommend relation for maximum horizontal acceleration for the central United States is

$$\log_{10} a_{\text{H}} \text{ (cm/sec}^2\text{)} = \begin{cases} -0.36 + 0.52 \text{ m}_{\text{b}} - 0.00 \log_{10} R & \text{R} \leq 15 \text{ km} \\ 0.84 + 0.52 \text{ m}_{\text{b}} - 1.02 \log_{10} R & \text{R} \geq 15 \text{ km} \end{cases}$$
(7)

with a standard error of estimate corresponding to a factor of about 2.0.

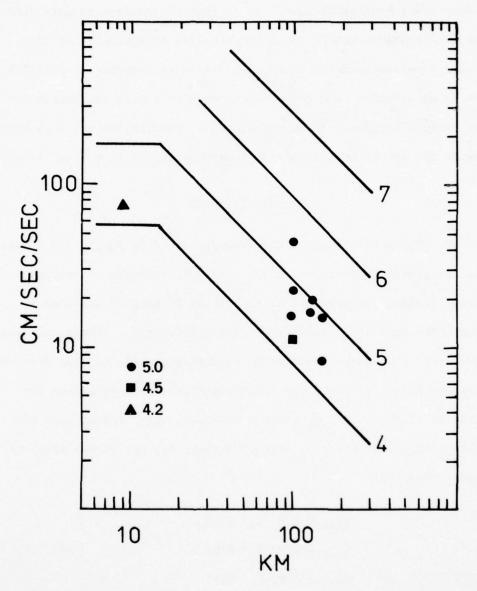


Figure 16. Central United States acceleration relation (Equation (7)) as a function of magnitude, m_b. Observed data from Herrmann¹⁴

70. Equation (7) was based on data from earthquakes and accelerograph sites in the Mississippi embayment. Thus Equation (7) may not in fact represent bedrock motions. It is also of interest to note that large accelerations result when Equation (7) is extrapolated to estimate accelerations due to the New Madrid earthquakes of 1811-1812. There is no existing data which can be used to verify the extrapolations to such large magnitude earthquakes. However, we can have confidence in the use of Equation (7) for earthquakes of $m_b = 6$ and less.

Maximum_Velocity

71. No correlations of the type performed by Murphy and O'Brien²⁵ exist for predicting peak velocity. Instead, concepts of source-spectrum scaling and theoretical results of Herrmann²⁶ are used to estimate the form of a maximum-velocity relationship. Extensions based on the work by Herrmann²⁶ and using reasoning similar to that used in Paragraphs 62 and 63 yield the following approximate relations for maximum acceleration, a_{max} , maximum velocity, v_{max} , and maximum displacement, d_{max} , in terms of seismic moment, M_{O} , and corner frequency of the source, f_{C} :

$$a_{max} = A M_o f_c^3 G(R)$$

$$v_{max} = B M_o f_c^2 G(R)$$

$$d_{max} = C M_o f_c G(R)$$
(8)

where the geometrical spreading factor G(R) is defined as

$$G(R) = \begin{cases} 1.0 & R \leq R_{O} \\ (R/R_{O})^{-1} & R \geq R_{O} \end{cases}$$
 (9)

If the source spectrum is assumed to have a high frequency asymptote of f^{-2} , and assuming that $f_c < 1$ Hz, the following relationships immediately follow for $R \ge R_O$

$$\log_{10} a_{\text{max}} = D + 0.5 m_b - 1.0 \log_{10} R$$

 $\log_{10} v_{\text{max}} = E + 1.0 m_b - 1.0 \log_{10} R$ (10)
 $\log_{10} d_{\text{max}} = F + 1.5 m_b - 1.0 \log_{10} R$

Implicit in this derivation are the assumptions that m_b is directly proportional to the logarithm of the source-spectrum level at $f=1~\mathrm{Hz}$, and also that the basic shape of the faulting displacement as a function of time is the same, except for simple time scaling.

72. As an attempt to test this theoretical relation, curves of maximum horizontal velocity are plotted as a function of distance in Figure 17. The coefficient E was chosen to fit through the m_b = 5 data of the 25 March 1976 earthquake in the New Madrid seismic zone. Equation (10) is strictly valid only for regions for which anelastic attenuation is small; otherwise it would remain valid only at shorter distance, preferably less than 60 km. Keeping this in mind, some California strong-motion data are plotted as a further test of the hypotheses. Paragraph 68. The m_b values estimated by Nuttli et al 2 were used.

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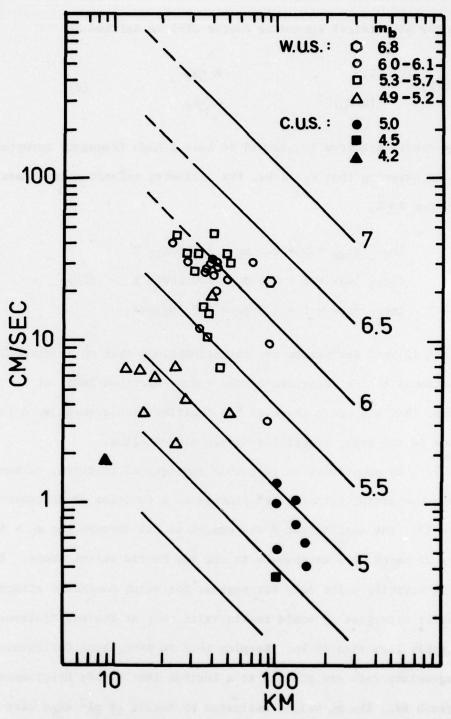


Figure 17. Maximum horizontal velocity as a function of distance and m_b (Equation (10)). Solid symbols are central United States data and closed symbols are selected western United States data, as a function of m_b

these earthquakes. The California strong-motion data are taken from a compilation by Chang 28.

73. The theoretical curves were fitted to the central United States data, which defined E = 2.92 in Equation (10). Only a fraction of the data in Chang²⁸ was plotted. The immediate conclusion is that the relation

$$log_{10} v_{max} (cm/sec) = -2.92 + 1.0 m_b - 1.0 log_{10} R$$
 (11)

fits the data quite well. Unfortunately, there are few data for m_b = 7. The Kern County, m_b = 6.8, earthquake is anomalous in that it has low ground motion velocities, perhaps indicating that it is a low stress drop event. An extrapolation of Equation (11) to m_b > 6.5 must be tested with real data from other sources, before one can feel comfortable in applying it to the central United States. Further work needs to be done in order to estimate the statistical confidence limits on the coefficients of Equation (11) as well as to estimate the lognormal standard deviation.

Maximum Displacement and Duration

74. A possible relation for peak horizontal displacement is given in Equation (10). However, the maximum displacements usually published in catalogs of strong-motion records are ordinarily contaminated by processing errors. Further research must be done on this point before displacement data can be used.

75. The duration of strong ground motion is difficult to specify because of differences in the basic definition of "duration." No statement on duration and its dependence upon magnitude and distance can be made for the central United States at the present time.

Theoretical work, now in progress, on the lines of Herrmann²⁶ may shed light on this parameter in the near future. At present, the best that can be done would be to use duration estimates based upon western United States strong motion data.

PART VI: SUMMARY AND CONCLUSIONS

- 76. The catalog of central United States earthquakes contained in Part III gives the date, origin time, epicentral latitude and longitude, epicentral intensity, felt area and body-wave magnitude for all known earthquakes strong enough to be felt and/or of mb greater than or equal to 3 which occurred since 1800. Statistical tests indicate the catalog is complete for all earthquakes of mb greater than 5. For lesser magnitude earthquakes the time interval for which the catalog is complete varies with source region and with magnitude.
- 77. A time interval extending back to 1800 is too short to ensure that the maximum-magnitude earthquake has occurred during it. That is, for most of the seismic source regions it is unlikely that the largest earthquake that can and will occur in the source region has happened since 1800. Thus there is a need to be able to predict the maximum-magnitude earthquake from the last 175 years of data. To do

this, it was assumed that the New Madrid region and the Charleston, South Carolina region have experienced their maximum-magnitude earthquakes in historic times, the former in 1811-1812 and the latter in 1886. These earthquakes were removed from the population of earthquakes which occurred in the two source regions since 1800, and magnitude-recurrence curves were constructed with the remaining data. In each case the extrapolation of these curves to a recurrence time of 1000 years gave a magnitude close to the observed magnitudes of the 1811-1812 and 1886 earthquakes. By this line of reasoning it is inferred that extrapolation of the recurrence curves for other source regions will give the maximum-magnitude earthquake when the recurrence time is 1000 years. (A recurrence time of 1000 years means that there is a 63% probability an earthquake of that size will occur within a 1000-year interval.) In this manner maximum-magnitude earthquakes were estimated for each of the seismic source regions of the central United States, as well as for the remaining area which is called the Residual region. The results are given in Table 21.

78. A recent paper by Ahorner and Rosenhauer 29 on seismic risk in the Upper Rhine graben of Germany and Switzerland also supports the contention of this report that the one-in-a-thousand year earthquake is a reasonable choice for the maximum-magnitude earthquake. Using a six-hundred year historical record of earthquakes, they proceed one step further and assign a zero probability to the occurrence of the extrapolated one-in-a-thousand year earthquake.

79. One of the principal purposes of this report is to give formulas which can be used to compute maximum acceleration and maximum velocity in bedrock for earthquakes of various magnitudes in the central United States. The desired relations are given by Equations (7) and (11). Figures 16 and 17 give plots of the equations, and present the results in graphical form. Equations (7) and (11) are derived relations, based in part upon theoretical formulations and in part upon observational data. The basic approach is to assume that log10 au, where aH is maximum horizontal acceleration, is proportional to the body-wave magnitude, m_b , and to \log_{10} R , where R is epicentral distance. The coefficients and the constant in the resulting equation are evaluated using the existing strong-motion data for central United States earthquakes. The results, for horizontal distances greater than the source depth, are shown to be consistent with what is known of attenuation in the region and with the manner in which the stress drop depends on seismic moment in the central United States. Thus, the empirical Equation (7) is shown to be consistent with theory, taken together with observational evidence on attenuation and seismic sourcespectrum scaling. Equation (11) for maximum velocity was developed from a theoretical knowledge of the behavior of the seismic source spectrum, with the constant in the equation chosen to fit the velocity data of the m = 5 earthquake of 25 March 1976 in the New Madrid seismic zone. Figure 17 shows that the resultant velocity-distancemagnitude equation also closely satisfies the California strong-motion

velocity data for earthquakes of m_b from 4 to 6.5. The scatter of the data points from the curves of Figure 17 is relatively small, and serves as a measure of the degree of uncertainty attached to Equation (11).

- 80. Data are lacking for strong-motion accelerations resulting from large magnitude earthquakes at near distances. For such a case it is necessary to consider the complex nature of the extended fault rupture process. Because of this the curves of Figure 16 are not extended to distances of less than 25 km for m_b = 6 earthquakes and to distances of less than about 40 km for m_b = 7 earthquakes. Resolution of this problem can only come when the ground motion of large magnitude earthquakes is recorded by accelerographs in the near field. Near-field data for the central United States can be expected to be similar to those for the western United States or other tectonic source zones because anelastic attenuation, which is the chief cause of differences in ground motion between the regions at larger epicentral distances, is unimportant at small distances.
- 81. In addition to collecting more strong-motion data for the central United States, it would be desirable to be able to more accurately outline the boundaries of the seismic source zones. This can be done by microearthquake and by geological studies. Progress towards the solution of this problem, as well as on accumulating more strong-motion data, will be slow, however, because of the relative infrequency of earthquakes in the central United States. Until that time it will be necessary to evaluate, on an individual basis, the

maximum-magnitude earthquake for sites near the boundaries of the seismic source zones.

82. The objective of this report has been to provide as complete a catalog of earthquakes as possible for the central United States, to determine the rate of seismic activity as well as seismic potential for the region, and to recommend new relations for the scaling of strong ground motion. The results of this report should be directly applicable for probabilistic risk analysis without much modification. On the other hand, direct use of these data in a deterministic approach must be tempered with caution because of the large areal extent of the source regions defined and the lack of observable causative faults in the region. The maximum-magnitude earthquake is defined as the one-in-athousand year earthquake for the entire source region. For deterministic studies, recognizing the small chance that this event will lie under the structure site, a smaller earthquake for design purposes should be chosen. Krinitzsky and Chang 24 have taken a conservative approach to this problem of the so-called "floating earthquake" by assuming that it can occur at the site, but have used their far-field relations between MM intensity and ground acceleration, velocity and displacement to estimate the site motion. Other possible approaches might be to use the one-in-a-hundred year earthquake as the maximum credible earthquake at the site, or to assume the magnitude of the maximum credible earthquake at the site is one unit less than that for the extended source region.

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APPENDIX A: Source Region Coordinates

- The polygonal source regions are described by specifying their corners in terms of latitude and longitude pairs. For consistency, these corners are ordered such that each successive pair is the next corner, when one progresses clockwise about the source region.
 - a. Anna, Ohio: (39.5, 85.0), (41.5, 85.0), (41.5, 85.0), (41.5, 83.0), (39.5, 83.0)
 - b. Northern Illinois: (41.0, 91.0), (43.0, 91.0), (43.0, 88.0), (41.0, 88.0)
 - c. Northern Great Plains: (41.0, 104.0), (47.0, 104.0), (47.0, 96.0), (41.0, 96.0)
 - d. Nemaha Ridge: (34.0, 100.0), (41.0, 98.0), (41.0, 95.0), (34.0, 97.0)
 - e. Wichita-Ouachita: (35.0, 103.0), (37.0, 103.0), (35.0, 90.0), (33.0, 90.0)
 - f. Wabash Valley: (39.0, 88.0), 39.6, 87.5), (39.6, 86.5), (38.5, 87.0), (36.5, 88.0), (37.5, 89.5)
 - g. Ozark Uplift: (37.0, 91.5), (39.0, 89.5), (38.5, 88.5), (35.5, 91.5)
 - h. New Madrid A: (35.5, 91.0), (37.0, 89.5), (36.5, 88.5), (35.0, 90.0)
 - New Madrid B: (35.5, 91.5), (37.5, 89.5), (36.5, 88.0), (34.5, 90.0) less region covered by New Madrid Λ.
 - j. Residual: (25.0, 110.0), (50.0, 110.0), (50.0, 80.0), (25.0, 80.0) less regions delineated above.

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State-of-the-art for assessing earthquake hazards in the United States; Report 12: Credible earthquakes for the central United States / by Otto W. Nuttli, Robert B. Herrmann, Department of Earth and Atmospheric Sciences, St. Louis University, St. Louis, Missouri. Vicksburg, Miss.: U. S. Waterways Experiment Station; Springfield, Va.: available from National Technical Information Service, 1978.

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